

# The influence of fiber size on the behavior of the araucaria pine nut shell/PU composite

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## Abstract

The use of araucaria pine nut shell in polymer composites may increase the pine nut value and help protect araucaria (*Araucaria angustifolia*) itself, which is an endangered species. The aim of this work is to study the influence of the size of pine nut shell fiber on the mechanical properties of composites made of this shell and polyurethane derived from castor oil. Composites with different polyurethane contents were manufactured with dried untreated pine nut shell sieved through 30 and 50 mesh sieves (0.6 and 0.3 mm, respectively). Composites were shaped by mechanical mixing of the components followed by hot pressing. Properties such as density, water absorption, and flexural strength were measured. Specimens were also characterized by SEM, FTIR, and TGA. The flexural strength of PU/0.3mm pine nut shell composites with 30% PU (wt%) was 57.7 MPa, and their water absorption was 7.37% after 24 hours of immersion.

**Keywords:** *araucaria pine nut shell, composite, castor oil, polyurethane, mechanical properties.*

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## 1. Introduction

The development of products with low cost, reduced energy consumption and life cycle sustainability is driven by the worldwide concern with the environment and human health<sup>[1-3]</sup>. Biodegradable composites are environmentally friendly<sup>[1]</sup>, can be made from renewable sources, and degraded by the action of microorganisms<sup>[2,4]</sup>.

Composites made of biodegradable polymers and reinforced by natural fibers are an attractive option, since these fibers have some advantages when compared to synthetic ones, such as lower density, lower cost, and lower abrasivity during manufacturing. Besides, natural fibers are derived from renewable sources, are not toxic, and do not cause environmental impacts<sup>[1,5-7]</sup>.

Fernandes et al.<sup>[8]</sup> analyzed the influence of silica nanoparticles on the compatibility between sisal fibers and high density polyethylene. They observed that thermal properties of HDPE did not change because of the presence of sisal fibers and silica nanoparticles in the composite. The different chemical treatments in sisal fibers and the presence of silica nanoparticles resulted in improved

mechanical properties and water uptake decrease in the composites, when comparing to HDPE.

Spadetti et al.<sup>[9]</sup> investigated thermal and mechanical properties of composites made of both virgin and recycled polypropylene reinforced with cellulose fiber. The results showed that recycled polypropylene composites with 30% (wt%) cellulose fibers and virgin polypropylene composites with 20% (wt%) of cellulose fibers had a significant increase in storage modulus values ( $E'$ ) and degree of crystallinity ( $\chi_c$ ), indicating a higher mechanical strength in these composites. However, the stiffness specimens of the material with 40% (wt%) of cellulose fibers decreased. These results were confirmed by SEM, where some agglomeration of the cellulose fibers within the matrix was observed. Both glass transition temperature ( $T_g$ ) and crystalline melting temperature ( $T_m$ ) of composites did not change.

Mano et al.<sup>[10]</sup> studied the morphological, mechanical, and thermal properties of composites made of polypropylene reinforced with curaua fibers treated with maleic anhydride grafted polypropylene. The use of PP-g-MA as a compatibilizer significantly increased fiber/matrix adhesion; however,

mechanical properties were only slightly improved when comparing to composites produced without compatibilizer.

Beltrami et al.<sup>[4]</sup> studied the morphological, mechanical, and thermal properties of composites made of PHBV and curaua fibers with alkaline treatment. Results indicate that the alkaline treatment improved the adhesion of the fibers to the matrix, which significantly improved the mechanical properties of the composites. However, NaOH concentrations of NaOH different from 5% may have a deleterious effect on the mechanical properties of the fibers and composites.

Mei & Oliveira<sup>[7]</sup> studied the morphological, mechanical and thermal properties and the biodegradability of composites containing chemically treated coffee grounds and poly( $\epsilon$ -caprolactone). Thermal analysis showed that the addition of coffee grounds increased the maximum peak of thermal degradation by 10°C when compared to pure polymer. Biodegradability was higher for specimens containing acetylated coffee grounds.

Load transfer from the polymer matrix to the fibers greatly depends on the matrix-fiber interaction<sup>[4]</sup>. Natural fibers are hydrophilic, while most polymer matrixes are hydrophobic<sup>[8,11]</sup>. As a result, the adhesion between those materials is compromised, decreasing the mechanical properties of the composite<sup>[5,6]</sup>. One possible way to improve such interaction if by modifying the surface of the fibers by means of physical<sup>[12,13]</sup> or chemical methods<sup>[4,5,7]</sup>.

Polyurethane derived from castor oil is a biodegradable polymer produced from renewable sources, and it is harmless to human health and to the environment, since no volatile organic compounds are liberated in its synthesis<sup>[6,14,15]</sup>. During polyurethane polymerization in the presence of vegetable fibers, crosslinks may result from the reaction of active hydrogens from hydroxyl or carboxyl groups from lignin and PU free isocyanate. Such reactions may improve matrix-fiber interaction, leading to better load transfer and enhanced mechanical properties. This is the reason no previous treatments on the fibers and no coupling agents are needed in this type of composites<sup>[11,16]</sup>.

Marinho et al.<sup>[15]</sup> studied physical and thermal properties of composites made of PU based on castor oil and bamboo particles without any previous treatment. This approach minimizes the negative impact to the environment, since a solvent free polymer is obtained. The association of PU and bamboo particles produced the expected effects, including a decrease in moisture content, swelling and water absorption of bamboo as PU content increased.

Zau et al.<sup>[17]</sup> analyzed the chemical, physical and mechanical properties of agglomerated panels made of cumaru wood residues with PU derived from castor oil. They produced panels with different amounts of residues (1000, 1300, 1500 g) and resin content (10, 12.5 and 15%). Higher mechanical properties were achieved for panels with 1500g of residue and 15% of resin, and the values exceed the minimum specified by the NBR 14810-3 (2006), confirming their potential in producing particleboards.

*Araucaria angustifolia* is a tree from southern Brazil<sup>[18]</sup>. It is an endangered species, and there are legal restrictions concerning the use of its wood; therefore, incentives are given to the commercialization of its seed, the pine nut<sup>[19]</sup>. Pine nut is a nutritious food, containing mainly starch and

low amounts of sugars and lipids in its composition<sup>[20]</sup>. About 700 tons/year of pine nut shell residue are disposed of in south Brazil<sup>[21]</sup>. The use of this pine nut shell in polymer composites can reduce the amount of discarded material in the environment and increase its value. *Araucaria angustifolia* is an endangered species, mainly because of illegal exploitation and commercialization of its wood. The use of pine nut shell may help to preserve the trees, since it can be a source of income and avoid cutting down trees. Composites made with pine nut shell can be used in handicrafts and furniture, replacing MDF, which has a significant impact on the environment.

The aim of this work is to evaluate the effect of pine nut shell size on mechanical, physical, and thermal properties of composites made of castor oil polyurethane and pine nut shell. Two different sizes of pine nut shell were used, i.e., those passing through 30 and 50 mesh (0.6 and 0.3 mm sieve opening), and the composites were produced with varying amounts of PU by means of mechanical mixing and hot pressing. Several characterization tests were carried out, namely: volumetric density, water absorption, flexural strength, thermogravimetric analysis (TGA), Fourier-transform infrared spectroscopy (FTIR), X-ray diffraction (XRD), and scanning electron microscopy (SEM).

## 2. Materials and Methods

### 2.1. Materials

Castor oil-based PU resins employed in this work were developed by the Group of Analytic Chemistry and Technology of Polymers – USP. Polyurethane is a bi-component resin obtained by the reaction of a polyol and an isocyanate terminated pre-polymer. Currently, both pre-polymer and polyol are produced by Cequil, from Araraquara-SP, Brazil. The pre-polymer used is based on the diphenylmethanodiisocyanate (MDI). Polyols are polyesters derivate from castor oil with different amount of functional hydroxyl groups. The pre-polymer was synthesized from diphenylmethanediisocyanate (MDI) and prepolymerized with polyols, also derived from castor oil, keeping a percentage of free isocyanate for later reaction. PU Polibond® is athermoset adhesive. Polymer preparation was made according to the supplier instructions. Pine nut shell was donated by Embrapa Florestas, from Colombo-PR, Brazil. The shell was crushed in a knife mill suited for grains and dry materials. Crushed shells were classified through 30 and 50 mesh sieves (0.6 and 0.3 mm aperture), dried at 100°C for 24 hours and kept in a desiccator until used. No chemical or physical treatments were performed in the fibers.

### 2.2. Composites production

Composites with 50%, 60%, and 70% of pine nut shell (wt%) were produced by mixing the pine nut shell to the castor oil polyurethane in a MH-100 series 6069 mixer (MH Equipamentos) 3200 rpm for 20s. The mixture was shaped in a hot press (Marconi Equipamentos, model MA 098/AR15, under 6 MPa pressure at 70°C for 20 minutes, which was sufficient to allow the system to cure.

### 2.3. Characterization of composites

The density of the composites was measured according to EN 323:2002 Standard, and the water absorption was determined according to EN 317: 2002 Standard. Tests were conducted at a room temperature. Five specimens of each composite were cut from a plate, as 50X50 mm samples with unsealed borders. The initial thickness (the thickness is measured close to the center of the specimen) was measured and the samples were weighted before being submerged in distilled water for 2 h. After immersion, the water on the surface of the samples was removed, and the samples were immediately weighed, measured, and immersed in water again. After 22 h they were removed, pat dried, measured and weighted again.

Flexural tests were performed according to the ASTM D790-03 standard in an EMIC DL10000 universal tester, with load cell of 20 kN and test speed of 5mm/min.

Scanning Electron Microscopy was performed in a Zeiss microscope, model EVO MA 15. Specimens were gold sputtered prior to observation. SEM was used to investigate the surface of fibers after drying and the fracture surface of the composites after flexural test.

Thermogravimetric analyses (TGA) were carried out in a Perkin Elmer STA 6000 thermo scale, and the following parameters were used: Specimen mass: 5.0 to 10.0 mg; Temperature range 30 °C to 800 °C; Heating rate 10 C/min; Flow of N2 atmosphere 100 mL/min.

FITR analyses were carried out in a Varian infrared spectrometer model 640-IR, equipped with a diamond ATR accessory from PIKE, with a resolution of 4 cm<sup>-1</sup>.

A Shimadzu X-ray diffractometer, model XRD-700, with Cu K $\alpha$  radiation, operating at 40 kV and 20 mA was used to analyze the crystallinity of the specimens. The degree of crystallinity was determined by the technique proposed by Hermans and described by Poletto<sup>[22]</sup>.

## 3. Results and Discussions

### 3.1. Density measurements

The density of the composites is shown in Table 1. It ranged from 1155.50 to 1214.08 kg/m<sup>3</sup>. According to Brasil et al.<sup>[23]</sup>, the density of the pine nut shell powder is 180 kg/m<sup>3</sup>. PU density is 1090 kg/m<sup>3</sup> and pine nut shell is 900 kg/m<sup>3</sup>.

The data shown in Table 1 indicates that independent of the amount of fiber and its size, the density vary slightly, and increases a little when compared to the PU.

**Table 1.** Composites density.

Sieve	PU (wt%)	Density (Kg/m <sup>3</sup> )
-	100	1090.00±0.03
0.6	30	1194.31±24.66
0.6	40	1155.50±57.30
0.6	50	1155.63±14.15
0.3	30	1200.64±21.80
0.3	40	1213.78±15.45
0.3	50	1184.55±29.31

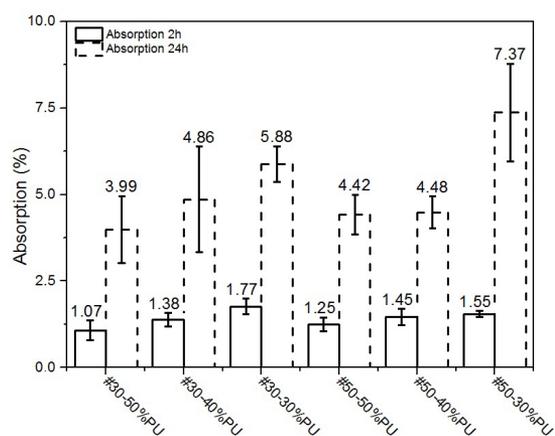
The density of the composite with the addition of pine nut shell powder is greater than the density of PU alone. According to the rule of mixtures, the density of the composite should be lower than the PU. Bubbles are generated during the production of PU because of the reaction of isocyanate with air humidity, as observed by Merlini et al.<sup>[16]</sup> and Marinho<sup>[15]</sup>. However, it was possible to obtain a slightly better densification of the composites because of the high speed (3200 rpm) of the mechanical mixing process, since the fine powder of the pine nut shell occupied the spaces of the bubbles generated in the polymerization process, thus allowing the incorporation of 70% of particles of 0.3 mm. The standard technique used to produce composites with thermoset matrix is manual mixing of the components followed by pressing. The technique employed in this work, i.e., mechanical mixing, allowed a greater incorporation of fine particles within the polymer matrix, increasing the density of the material when compared to neat PU.

### 3.2. Water absorption determination

The results obtained from the water absorption test for 2 and 24 hours for the composites with different fiber particle sizes are shown in Figure 1.

Our data indicate that water absorption increases with time, fiber content and decreasing particle size. This is to be expected since water absorption is attributed to the lignocellulosic component. So, water uptake should increase with the amount of fiber and its surface area. Even though the standard used in this work suggest that water uptake measurements should be made after 2h and 24h of immersion, we performed measurements up to saturation, as the ASTM D570 standard suggests. We observed that composites absorb water rapidly within the first 24 hours, and after that, a saturation level of 12.5% is reached for a sample with 50% PU, and no further water uptake is observed, even after 15 days of immersion.

Composites with 0.6 mm and 0.3 mm fibers and 50% PU showed the lowest water absorption in 2 and 24 hours immersion, and this is attributed to the higher amount of PU of these composites.



**Figure 1.** Water absorption test results. 2 and 24 hours of test for composites with 0.6 mm (#30) and 0.3 mm (#50) fibers.

Water absorption is lower for the composites made with 0.6 mm fiber. Bigger fibers have less surface area, resulting in less water absorption. Composites made of 0.3 mm fiber and 40% PU and 50% PU showed very similar water absorption values.

Water absorption occurs only by the pine nut shell particles, because PU does not absorb water<sup>[15]</sup>. The values obtained indicate that the fibers were covered by PU efficiently regardless of the amount and granulometry of the fibers used and this is attributed to the mixing technique employed here. Marinho<sup>[15]</sup> has studied the water absorption of manually mixed PU and bamboo composites using the same PU employed here and obtained water uptake values of 22.9% for composites made with 80% (wt%) of 2.7 mm bamboo fibers. Measurements were made according to the ASTM D570 standard at room temperature.

### 3.3. Flexural strength measurements

The flexural strength of the composites is shown in Figure 2. The flexural strength of PU is 42 MPa<sup>[11]</sup>, and the highest flexural resistance was obtained for the composite made with 0.3 mm pine nut shell and 30% PU. When compared to PU, the increase in flexural strength was 27%.

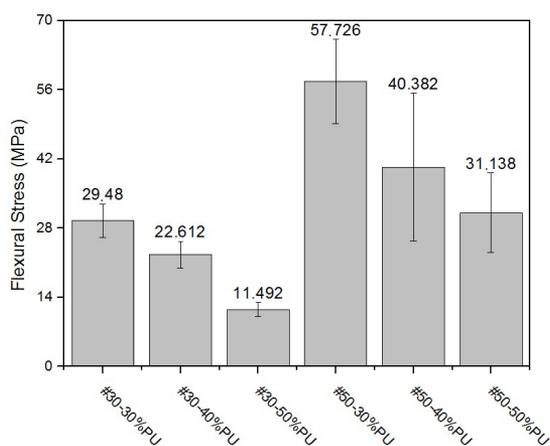


Figure 2. Flexural strength of the composites.

The data shown in Figure 2 indicate that the flexural strength of the composites increases with increasing fiber content and decreasing filler particle size. This is associated with improved packing of finer fibers, as shown in Figure 3. Vasco et al.<sup>[11]</sup> and Merlini et al.<sup>[16]</sup> observed that an interaction between hydroxyl groups from the fibers and PU isocyanate occurs, promoting chemical adhesion between the polymer matrix and the reinforcement. Smaller fibers favor packing, distribution and homogenization of the reinforcement within the matrix, resulting in better adhesion between materials<sup>[24]</sup>.

The fibers were not treated to improve the interface with the PU, and even so displayed higher flexural strength values than those of other composites made with natural fibers, such as the composite developed by Zau et al.<sup>[17]</sup>, that found flexural strength of 14 MPa for composites made with 85% sugarcane bagasse and castor oil polyurethane adhesive-based particulate. This shows that the mixing technique is efficient for the production of fine particulate composites with larger amounts than usual.

### 3.4. SEM

The micrographs of the fracture surfaces after three-point flexural test of composites made with 0.6 mm pine nut shell and 30% and 50% PU are shown in Figures 4a and 4b, respectively. In Figure 4a, a good fiber-matrix interface can be observed, as well as the presence of voids resulting from the fibers that were detached from the matrix during the tests. The fracture of the PU matrix and the presence of bubbles can also be observed.

For the composite with 50% PU (Figure 4b), the good fiber-matrix interface, as well as the voids from detached fibers, can also be observed. PU displayed brittle fracture, as demonstrated by the mirror-like areas close to stress concentrators such as bubbles and impurities of the surface of the fiber. The reduction in the composite mechanical strength could also be attributed to these characteristics.

Figures 5a and 5b show the fracture surfaces after bending test of composites made with 0.3 mm pine nut shell and 30% PU and 50% PU, respectively. In Figure 5a, it is not possible to observe the presence of voids or holes

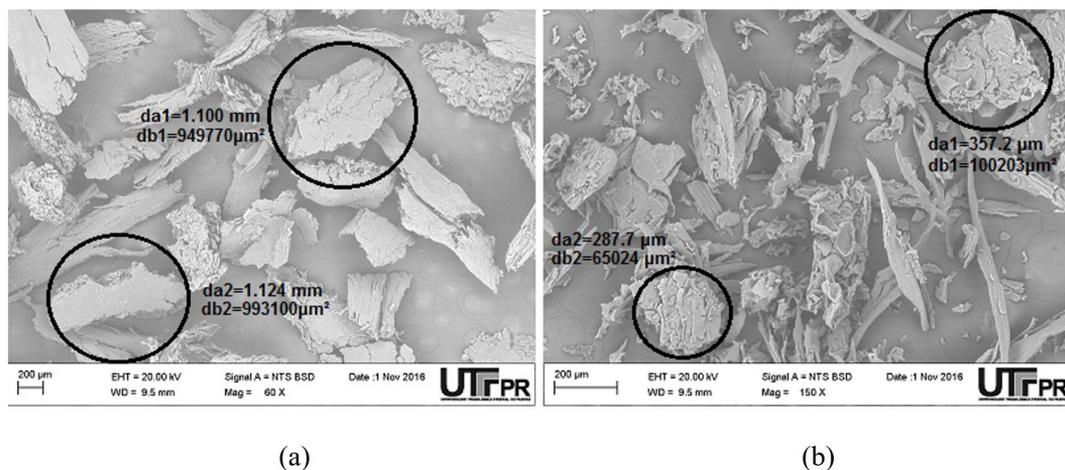
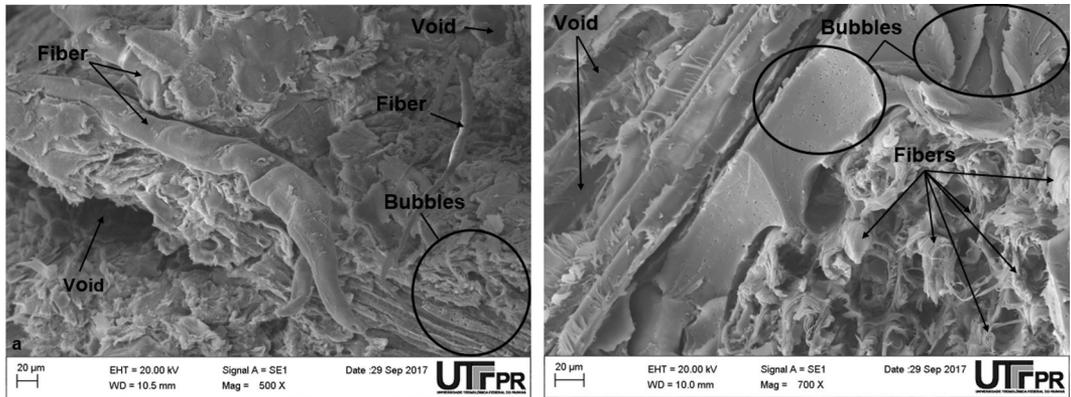


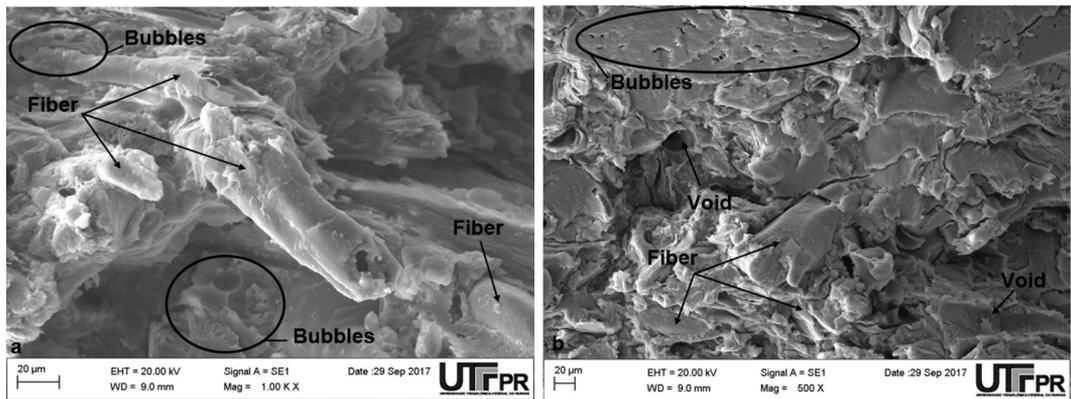
Figure 3. SEM micrographs of 0.6 mm (a) and 0.3 mm (b) particles.



(a)

(b)

Figure 4. SEM micrographs of the fracture surface of 0.6 mm composites: (a) 30%PU, (b) 50%PU.



(a)

(b)

Figure 5. SEM micrographs of the fracture surface of 0.3 mm composites: (a) 30%PU, (b) 50%PU.

in the fiber-matrix interface, indicating that the fibers were well covered by the polymer and some chemical interaction between the components might have occurred. This increases the adhesion between fibers and polymer, improving mechanical properties by means of a better distribution of mechanical loads. Some small bubbles can also be observed throughout the composite. In Figure 5b, the interaction between the fibers and the matrix can be observed, as well as the presence of voids resulting from fiber detachment. PU fracture is brittle, and there are bubbles all over the matrix. Although the homogenization technique has been efficient to promote the incorporation of the fiber into the matrix, it does not avoid the formation of small bubbles, which are inherent to the PU production process.

### 3.5. TGA

The results from the thermogravimetric analyses for PU and pine nut shell are shown in Figures 6a and 6b, respectively.

Two distinct events can be observed for the PU, the first one occurring between 250°C and 350°C with a mass

loss of 40%. In this temperature range, the urethane bonds are broken<sup>[25]</sup>. The second event takes place between 350°C and 500°C with a mass loss of 60%, and this is attributed to the decomposition of the ester bonds present in polyol<sup>[26]</sup>.

Regarding the pine nut shell, an initial mass loss event at 30°C is observed, which is associated with the loss of absorbed water, typical of lignocellulosic materials<sup>[7]</sup>. In the range from 170°C to 295°C, there is another mass loss event related to the degradation of hemicellulose<sup>[5]</sup>. From 295°C to 330°C, cellulose degrades<sup>[27]</sup>, while lignin degrades between 330 and 500°C<sup>[28]</sup>. The remaining 27% of mass can be considered carbonaceous residues.

In Figure 7, the TGA and DTG curves of 30 mesh and 50 mesh composites are shown. From the figure, it is possible to observe that the thermal stability of the composites lies between those of PU and pine nut shell. The first event occurs between 50°C to 150°C, and it is related to the presence of water [11]. The next event occurred between 150°C and 394°C and might have happened because of the degradation of the pine nut shell. The third event occurs from 394°C to 500°C and is probably related to the degradation of the PU.

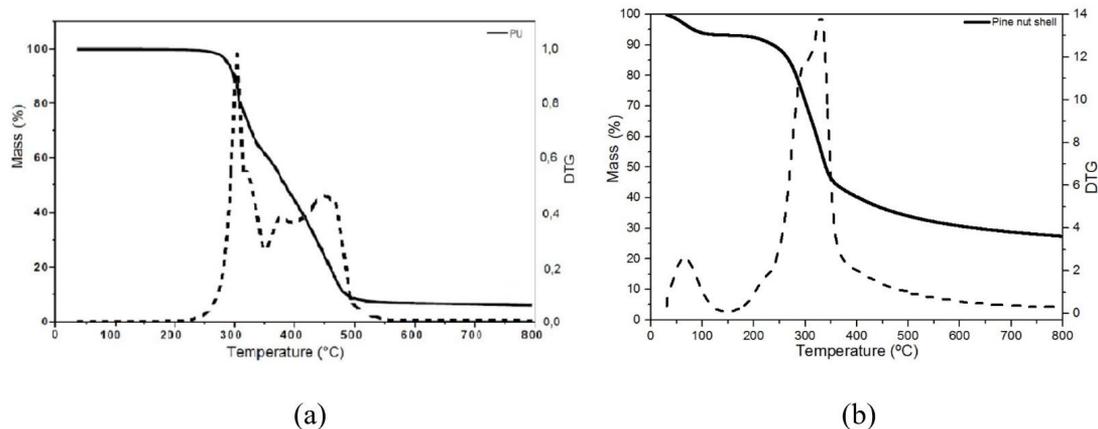


Figure 6. Thermogravimetric data for (a) PU and (b) pine nut shell.

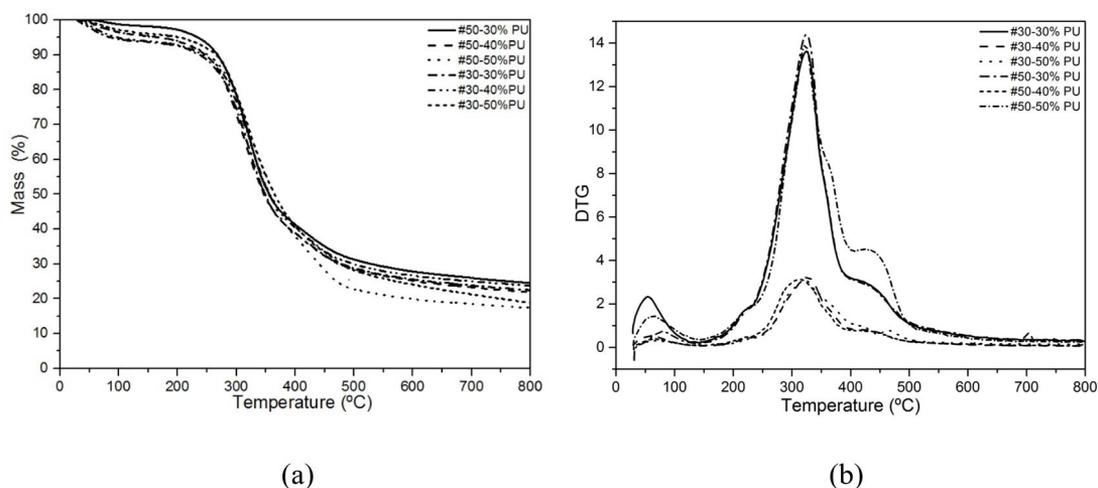


Figure 7. (a) TG and (b) DTG curves of 0.6 mm (#30) and 0.3 mm (#50) composites.

Particle size does not influence the thermogravimetry of the composites. The initial mass loss of the composites occurs around 150 °C, which is expected, since the thermal stability of the fibers of pine nut shell is around 170 °C.

### 3.6. FTIR

FTIR spectrograms of PU and pine nut shell are shown in Figure 8. For PU, an O-H band is observed at 3320 cm<sup>-1</sup>. The bands at 2920 and 2850 cm<sup>-1</sup> are associated with C-H symmetrical and asymmetrical stretching<sup>[27]</sup>. The isocyanate band is located at 2270 cm<sup>-1</sup><sup>[16]</sup>, and the urethane bands at 1700, 1596, and 1520 cm<sup>-1</sup> are related to the C=O and N-H stretching, and they tend to increase with the crosslinking of the polyurethane chains<sup>[16,29]</sup>.

For the pine nut shell, a band at 3340 cm<sup>-1</sup> associated to lignin phenols and cellulose and hemicellulose hydroxyls can be observed<sup>[30]</sup>.

The band at 2930 cm<sup>-1</sup> is related to the C-H bond stretching present in cellulose and hemicellulose<sup>[5]</sup>. The peak at 1610 cm<sup>-1</sup> is related to C=O carbonyl bonds of the lignin<sup>[16]</sup>, while the peak at 1024 cm<sup>-1</sup> corresponds to the C-H aromatic group and to the stretching of primary alcohols of lignin<sup>[5]</sup>.

The spectrograms of 0.6 mm and 0.3 mm composites are shown in Figure 9a and Figure 9b respectively. There was a reduction in the intensity of the NCO and OH peaks of the composites. Such reduction might indicate a chemical affinity between O-H and N-C-O groups of the materials which the composites are made of.

### 3.7. XRD

The XRD diffractograms of PU, pine nut shell fibers, and composites (both 0.6 and 0.3) are shown in Figure 10.

Polyurethane results from the chemical reaction between an isocyanate and a hydroxyl group. In this polymerization, a compound containing two or more isocyanate groups per molecule reacts with a polyol or a polyfunctional alcohol. Any changes in the polyol and pre-polymer ratio (–NCO/–OH) cause substantial morphological changes in the PU chains, leading to modifications in mechanical properties of the material. The degree of crosslinking is controlled by the isocyanate group (–NCO) of the pre-polymer and by the hydroxyl group of the polyol, and, in the composites with pine nut shell, a reaction with the OH of the pine nut shell particles also occurs.

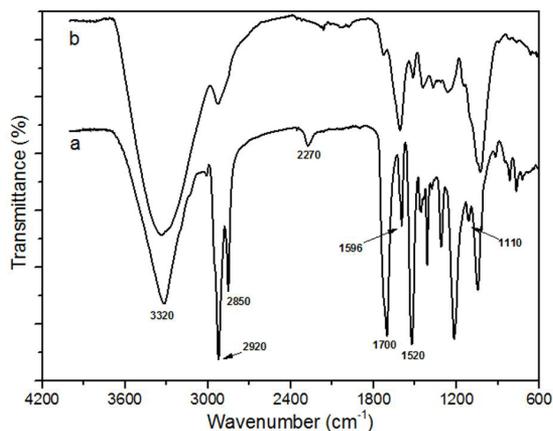


Figure 8. FTIR spectra of (a) PU and (b) pine nut shell.

As demonstrated in Figure 10, the diffraction profiles show an amorphous broad shoulder, diffused diffraction with a maximum at  $2\theta = 20^\circ$ . It is likely that some soft segment-hard segment phase mixing could occur in the system disturbing the soft segment crystallization<sup>[26,29]</sup>. This may account for the broader diffraction peaks shown in the diffractograms. For ordinary synthetic polymers, the nonuniformity of the molecules makes it impossible to form perfect single crystals. As a result, amorphous and crystalline phases are present in a real polymers, and these entities have complex organization.

In the pine nut shell diffractograms, peaks at  $16^\circ$  and  $22^\circ$  are observed, corresponding to the amorphous and crystalline regions of cellulose, respectively<sup>[31]</sup>. Such behavior is similar to semicrystalline structures.

The degree of crystallinity of the composites are shown in Table 2, The determination of the amorphous to crystalline percentage was obtained from peak area ratios. It can be

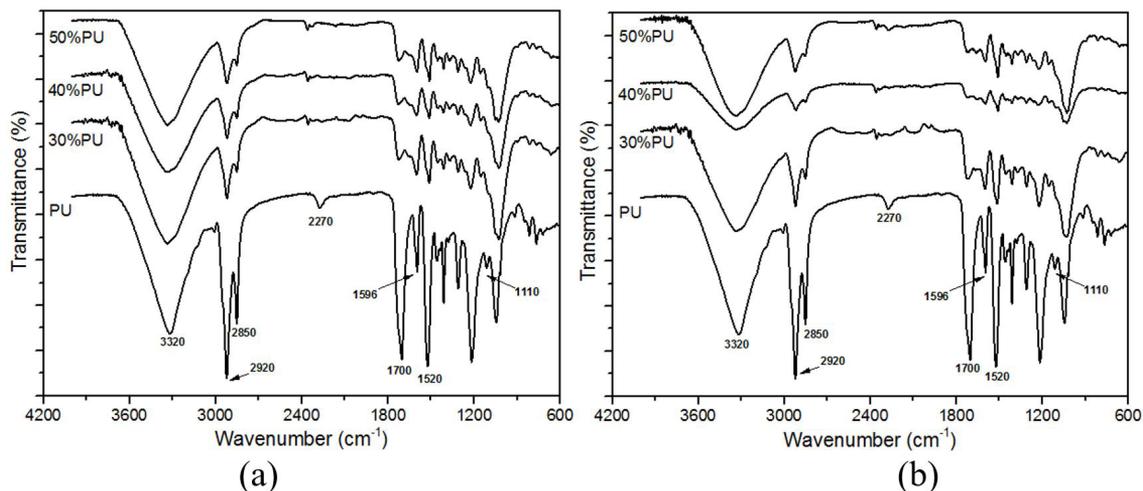


Figure 9. FTIR spectra of PU and composites: (a) 0.6 mm and (b) 0.3 mm.

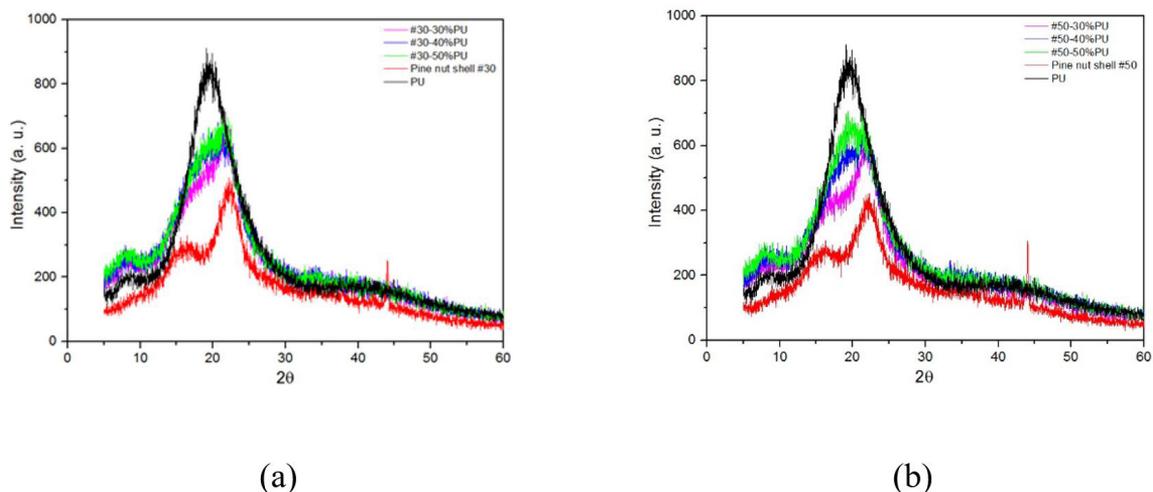


Figure 10. XRD diffractograms of PU, pine nut shell fibers, and composites: (a) 0.6 mm (#30) and (b) 0.3 mm (#50).

**Table 2.** Degree of crystallinity.

Sieve	PU (%)	X <sub>c</sub> (%)
0.6	0	36
0.6	30	32
0.6	40	34
0.6	50	31
0.3	0	36
0.3	30	32
0.3	40	32
0.3	50	32
-	100	31

observed that the composites display a small increase of crystallinity when compared to neat PU, indicating that structural changes occurred during the production process. The results indicate that filler particle size does not affect the degree of crystallinity.

#### 4. Conclusions

The aim of this work was to investigate the mechanical, physical and thermal properties of properties of PU/pine nut shell composites as a function of fiber content and granulometry. Density was higher for composites made with finer fibers, and water absorption increased with time, fiber content and decreasing particle size. Flexural strength was higher for composites with higher amount of fibers and smaller sizes. A good fiber-matrix interface, as well as the presence of micro bubbles, which are inherent of the PU production process, was shown by the SEM micrographs. TGA analyses showed that PU and all composites were thermally stable up to 150°. The reduction in the intensity of the NCO and OH peaks observed in FTIR analyses indicates reaction between these groups. The results indicate that the composite degree of crystallinity was not affected by filler particle size.

#### 5. Acknowledgements

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