

## Diamond Films on Stainless Steel Substrates with an Interlayer Applied by Laser Cladding

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The objective of this work is the Hot Filament Chemical Vapor Deposition (HFCVD) of diamond films on stainless steel substrates using a new technique for intermediate barrier forming, made by laser cladding process. In this technique, a powder layer is irradiated by a laser beam to melt the powder layer and the substrate surface layer, to create the interlayer. The control of the laser beam parameters allows creating homogeneous coating layers, in rather large area in few seconds. In this work, the silicon carbide powder (SiC) was used to create an intermediate layer. Before the diamond growth, the samples were subjected to the seeding process with diamond powder. The diamond deposition was performed using Hot-Filament CVD reactor and the characterizations were Scanning Electron Microscopy, X-ray diffraction, Raman Scattering Spectroscopy and Scratch Test.

**Keywords:** Laser Cladding, HFCVD, Diamond Film

### 1. Introduction

CVD diamond films on steel substrates present great interest because of their unique properties. CVD diamond film as a protective film produces an increase in surface hardness, thermal conductivity; on the other hand, it decreases low friction coefficient. Steel is widely applied in the industry. Diamond coating on steel may provide many applications because of diamond intrinsic properties. On the other hand, there are still difficulties at adhesion between diamond films and steel substrates.

Direct synthesis of diamond film on steel has been limited because of at least three major obstacles<sup>1,2</sup>. First iron is not a catalyst for CVD diamond growth, which forms graphite layer on the surface instead of a diamond. Second, the carbon from the gas phase has high diffusion rate into the steel at CVD temperatures, decreasing diamond nucleation. Third, the AISI 304L has a higher thermal expansion coefficient ( $17.3 \times 10^{-6} \text{ K}^{-1}$ ) than the diamond ( $0.8 \times 10^{-6} \text{ K}^{-1}$ ) resulting in a mismatch, this fact increases the residual stresses in a film-substrate interface, leading to a poor adhesion.

There are many alternatives described in literature to reduce these three issues, as the surface modifications<sup>3</sup> and the deposition of intermediate layers<sup>4,5</sup> to block the iron diffusion to the substrate surface and the carbon diffusion from the gas phase into the steel, during the CVD diamond deposition, as well to reduce residual stresses effect between the diamond and the steel.

The literature shows interlayers to achieve adherent diamond films on steel substrates, such as Si<sup>6</sup>, CrN<sup>7</sup>, TiC<sup>8</sup>. Lin et al.<sup>9</sup> obtained good adhesion on steel by electroplated Ni interlayer. Fan et al.<sup>10</sup> reported adherent diamond coating on steel with a titanium interlayer by DC sputtering, pull-off tests revealed the diamond coating adhesion was better than 13 N/mm<sup>2</sup>. Buijnsters et al.<sup>11</sup> showed that CrN interlayer, by arc PVD, was efficient to deposit diamond film onto high-speed steel substrate; on the other hand, CrN intermediate barrier didn't provide a uniform diamond deposition for the 316 stainless steel.

This study explores the use of SiC interlayer for diamond deposition by laser cladding process. The barrier creation by laser cladding process is innovative. Process objective<sup>12</sup> is the deposition of a molten layer on the substrate surface. The process uses power laser beam to melts the powder on the surface, forming an adherent coating to the substrate<sup>13</sup>.

### 2. Experimental

The substrates for diamond coating were AISI 304L steel disks with of 25.4 mm x 3 mm (diameter x thickness). The radiation source for laser cladding was a carbon dioxide laser (Synrad - SH) with the output power of 50 W and beam diameter of 300  $\mu\text{m}$ . The beam intensity was 70 kW/cm<sup>2</sup>. The SiC powder was commercially available silicon carbide powder (Treibacher Schleifmittel Brasil). SiC average grain size was 4  $\mu\text{m}$  in all experiments

Table 1 shows the parameters used in the laser to create SiC intermediate layer on steel.

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**Table 1.** Laser cladding parameters.

Laser Parameters	1-SiC layer	2-SiC layer	3-SiC layer
Resolution (dots per square inch)	600	600	600
Number of heating cycles	2	2	2
Beam scanning speed (mm/s)	50	100	100
Atmosphere	N <sub>2</sub> – 5l /min flow	N <sub>2</sub> – 5l /min flow	N <sub>2</sub> – 5l /min flow

We employed two-step process in laser cladding. The first step consists of powder application by air gun, followed by laser incidence (second step). For 3-layer SiC, both the powder pulverization and laser irradiation were repeated 3 times, respectively.

Before CVD diamond deposition process, we introduced the seeding process that introduces diamond seeds as nuclei for the CVD diamond growth. The nucleation mechanism of diamond particles was based on ESA (Electrostatic Self-Assembly) process<sup>14</sup>. The first stage was sample immersion for 30 minutes in an aqueous solution with PDDA {- Poly (diallyldimethylammonium chloride)}. The last stage was immersion in a aqueous solution containing 4 nm dispersed diamond powders and the anionic polymer PSS - (Poly (sodium 4 - styrenesulfonate), for a period of 30 min<sup>15,16</sup>. After each stage, we washed the sample in DI water.

Diamond film deposition was performed in a HFCVD (Hot Filament Chemical Vapor Deposition) reactor. A set of 6 tungsten filaments with diameter of 125  $\mu\text{m}$ , kept at a temperature of around 2200  $^{\circ}\text{C}$  was the activation region. The distance between the filaments and the sample was at 5 mm. During the deposition, the substrate surface was 630  $^{\circ}\text{C}$  to lessen thermal stress induced by the difference in thermal expansion coefficients between diamond film and the substrate. To get a better anchoring of diamond film, we used TMCVD (Time Modulated Chemical Vapor Deposition) process<sup>17</sup>. This method consists of altering the methane concentration from low to high at predetermined times.

At the beginning of the diamond deposition process, samples were subjected for 20 minutes in a typical concentration of microcrystalline diamond (MCD), 2 % CH<sub>4</sub> dissolved in hydrogen at a 100 sccm total flow rate and 50 Torr constant pressure, to stabilize the process and the growth temperature. In the first modulation, the methane percentage was 6 % dissolved in hydrogen for 15 minutes. The second modulation was after two hours of MCD typical concentration growth, with the same concentrations described in the first. The time deposition was 3h.

Scratch test (UMT, CETR) evaluated adhering silicon carbide layer on the substrate surface. X-ray Diffraction (Panalytical X'pert Pro) analyzed phase quantitative in the laser cladding process. Qualitative analysis was made by Scanning Electron Microscopy (JEOL JSM-5310), FEG-SEM (Mira 3-Tescan) and SEM (Vega-Tescan). Raman Scattering Spectroscopy (Renishaw 2000) with an argon laser

excitation (514.5 nm) analyzed compressive residual stresses of diamond film. Rockwell Hardness Tester (Wilson J 3R) with the hardened steel ball of 1/8 inch diameter evaluated diamond coating adhesion on steel.

### 3. Results and discussion

Figure 1 shows the X-ray diffractogram of AISI 304L substrate with the characteristic peaks of the austenite phase<sup>18</sup>. The radiation wavelength is 1.5418740  $\text{\AA}$  (Cu-K $\alpha$ ).

This steel has a high chromium and lower carbon content, with a typical composition of 8% Ni, 18%Cr, 0.05%C, 0.6%Si, 1%Mn and the balanced being Fe<sup>19,20</sup>. The thermal expansion coefficient of austenitic steel is higher than diamond film. This difference results in the tendency to diamond film fragmentation. Diamond film coating is a prosperous method to change the wear resistance of steel surface and to make further functionality.

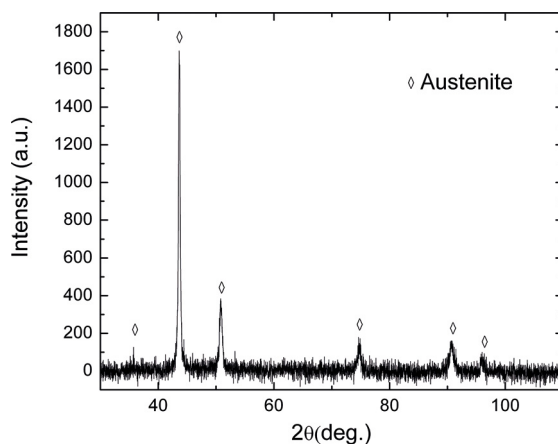
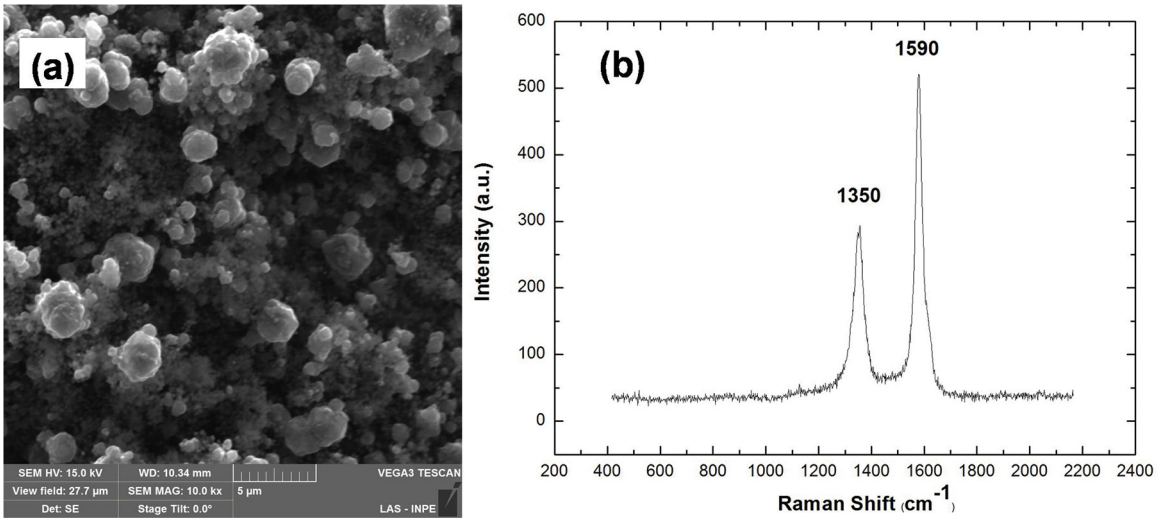
**Figure 1.** X-ray diffractogram of the AISI 304L sample.

Figure 2(a) shows the morphology of diamond film grown on bare steel. The time deposition was 3h and surface temperature was 630 $^{\circ}\text{C}$ . It can be seen some diamond spherical particles on loose graphite soot. Some diamond nuclei coalesced and grew on the top of graphite soot, but they are under free-standing and can be removed easily. The figure 2(b) shows the characteristic Raman spectrum. In addition, the figure shows two bands centered at 1350 and 1590  $\text{cm}^{-1}$ . These bands correspond to the D-band and G-band of graphite<sup>21</sup>, respectively.



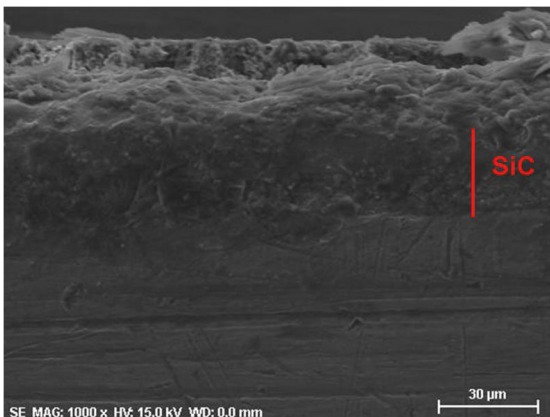
**Figure 2.** Diamond film on bare steel. (a) SEM image of diamond film on bare steel and (b) Raman spectrum of diamond film on bare steel.

Direct deposition of diamond film on bare steel leads to graphite soot creation due to iron catalytic effect in the graphite preferential nucleation. Intermediate layers are required to solve this problem.

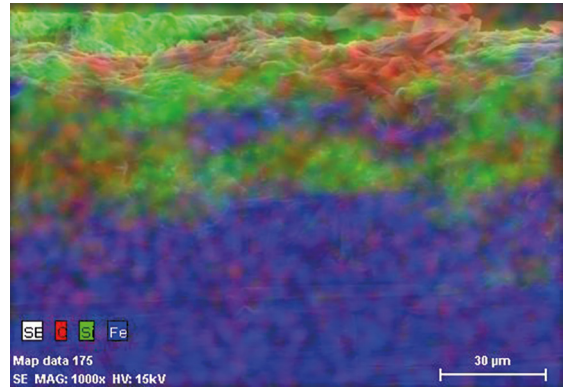
Figure 3 shows the sample cross section after laser cladding process.

It can be noted the formation of a SiC intermediate layer with a granular structure on the steel substrate surface. The layer thickness was about 30 microns. During laser irradiation, a thin layer applied on the substrate generates total powder sublimation; on the other hand, a thick layer does not cause heat transfer, from the laser beam, to the substrate. It is important to note that three layers were fully sintered by laser incidence, thus it is not possible to distinguish them. In addition, the image does not show cracks in the coating. Figure 4 exhibits the interface elements mapping between the SiC layer and the substrate.

The elemental mapping technique provided a spatial distribution of the chemical elements present at the interface. The interface elements did not indicate a large diffusion



**Figure 3.** SEM image of AISI 304L cross section after laser cladding process.



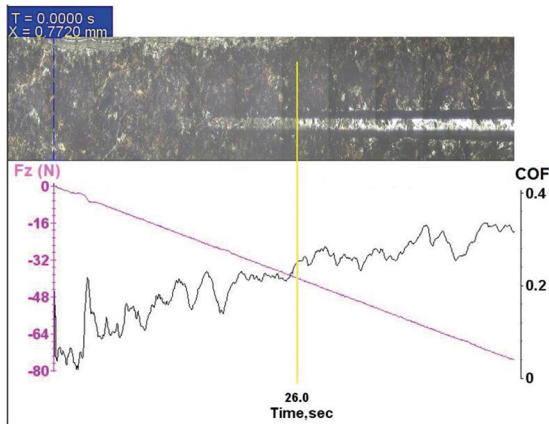
**Figure 4.** SEM image of the interface elemental mapping at interface.

between the SiC and AISI 304L (Fe) elements. The diffusion rate at the interface depends on the laser energy density<sup>22</sup>. Although the higher migration of iron atoms into the SiC interlayer decreases the barrier effectiveness, there is a need to create a diffusion pair (SiC and Fe elements) in order to form a metallurgical bond.

Figure 5 attests scratch test.

The scratch test evaluated the adhesion between SiC interlayer and steel substrate. The value of normal force, at which the first failure of SiC interlayer is detected by photographic camera, was 41 N. The intermediate layer must withstand the steel contraction during reactor cooling, in fact, behaving as a binding layer between the steel and the diamond. The high value of normal force can be related to strong metallurgical bond at a interface, formed during laser irradiation.

The surface roughness values of SiC intermediate layer were  $R_a=1.80 \mu\text{m}$ ,  $R_q=2.61 \mu\text{m}$  and  $R_z=6.77 \mu\text{m}$ . Laser incidence generates the sintering or semi-sintering of SiC grains. Then, the laser cladding forms intermediate barrier



**Figure 5.** Graphical representation of the critical load ( $F_z$ ) value.

with high surface roughness and, during the early diamond deposition stage, the diamond nuclei grow inside the SiC surface roughness, generating the interlocking action.

Figure 6 shows the morphology of diamond film grown on stainless steel.

The efficiency of diffusion process blocking is evidenced by the diamond growth. Diamond coating on SiC layer is uniform without spallation, the triple interlayer inhibited the carbon diffusion and thus, the substrate was not carburized. The film presents good nucleation, with uniform distribution, which presents granular structure, formed by grains coalescence. At higher magnification, letter (b), the image reveals clusters of diamond grains in nanometric scale<sup>23</sup>.

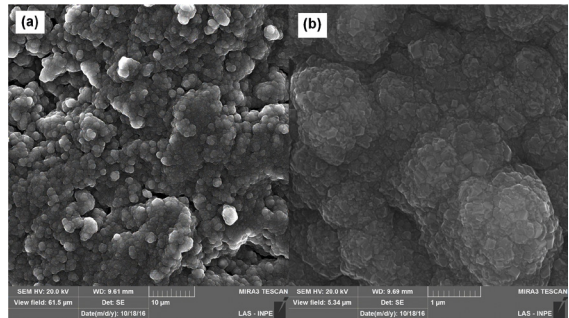
Figure 7 shows the characteristic Raman spectrum of the film grown on the AISI 304L substrate for 3 h.

The Raman spectrum shows a peak centered at  $1334\text{ cm}^{-1}$ , a typical characteristic of the diamond structure, shifted of about  $2\text{ cm}^{-1}$  from the diamond characteristic peak ( $1332\text{ cm}^{-1}$ ). It is correlated with residual stress in the diamond lattice<sup>24</sup>, which produces a compressive stress in the deposited diamond film.

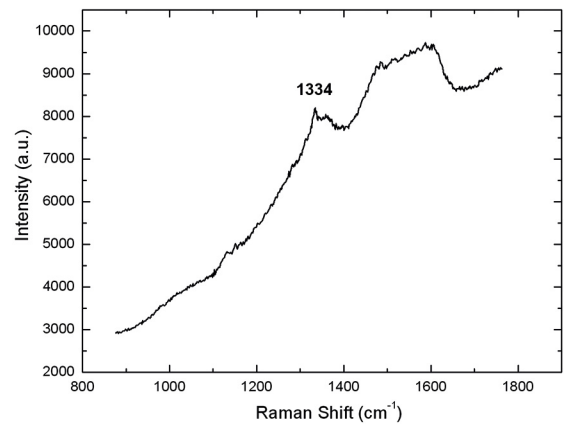
The shoulders at  $1140\text{ cm}^{-1}$  and  $1490\text{ cm}^{-1}$  have been related to transpolyacetylene (TPA) presence at the grain boundaries, both of them are found in NCD films<sup>4</sup>. The spectrum shows the D-band of graphite ( $1350\text{ cm}^{-1}$ ), which appears because of  $\text{sp}^2$  disorder. Further, the Raman signal corresponding to  $\text{sp}^2$  amorphous carbon, so-called G-band of graphite, is observed near, at  $1580\text{ cm}^{-1}$ , its low intensity shows a high purity diamond film grown on steel<sup>25</sup>. The NCD growth reduces residual stress in diamond films; which is an important fact since the higher stress leads to a diamond film delamination<sup>26</sup>.

The figure 8 shows the X-ray diffractogram after diamond growth.

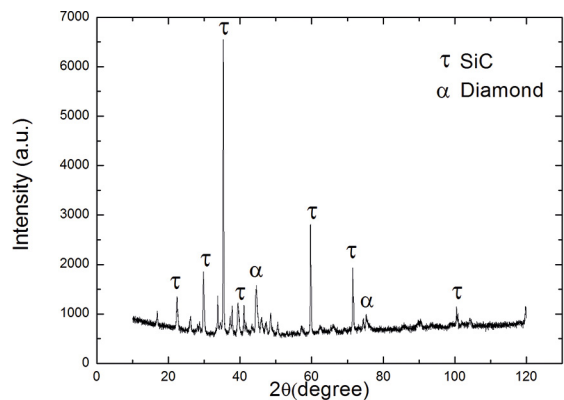
From the diffractogram, it can be inferred that SiC phase is higher peak intensity after diamond growth. The appearance of diamond peak confirms the diamond deposition. The



**Figure 6.** FEG-SEM image of diamond film on AISI 304L with SiC interlayer



**Figure 7.** Raman spectrum of diamond film on AISI 304L with SiC interlayer.



**Figure 8.** X-ray diffractogram of the diamond film on steel.

SiC intermediate barrier blocked the iron diffusion as no graphite peak is seen.

Figure 9 shows Rockwell indentation test on diamond film on steel.

The Figure 8 (a) and (b) show diamond coating after indentation at a load of 100 and 150 kg, respectively. In both, there weren't delamination and cracking of diamond coatings around the prints. It is correlated with high diamond film adhesion

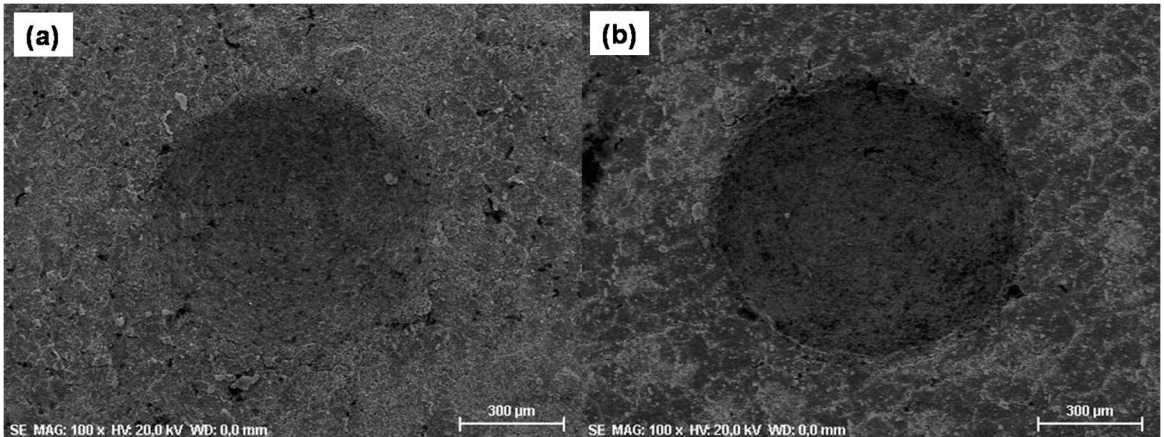


Figure 9. Rockwell indentation test of (a) 980 N (b) 1470 N.

onto substrate<sup>4</sup>. In addition, the figure shows small concentric cracks around the print, compressive stress of diamond film inhibited radial cracks formation running in concentric cracks<sup>27</sup>.

From these results, it is possible to indicate that laser irradiation provided an excellent metallurgical bond with the substrate. In addition, SiC interlayer successfully suppressed the high carbon solubility into the bulk steel substrate and catalytic the effect of iron on graphite soot formation. In addition, SiC has thermal expansion coefficient intermediate between diamond and steel, which reduced the residual stress at an interface. Enhanced adhesion of the diamond film to the steel was guaranteed because of SiC interlayer. Laser cladding features a promising method to create the intermediate barrier for steel substrate. Additional experiments showed the SiC layer effectiveness as an intermediate barrier for diamond deposition.

#### 4. Conclusions

In this work, adherent diamond films were deposited on AISI 304L substrate using an intermediate barrier, made by laser cladding. The interlayer blocked the iron diffusion to the substrate surface and carbon diffusion from the gas phase into the steel during the CVD diamond deposition. Further, the silicon carbide layer behaved as a binding layer, with intermediate mechanical and thermal properties between steel and diamond, this fact lessened the three main adherence problems between the diamond film and steel substrate.

#### 5. Acknowledgments

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