

## Determination of $U_3O_8$ in $UO_2$ by infrared spectroscopy

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### Abstract

The oxygen-uranium (O-U) system has various oxides, such as  $UO_2$ ,  $U_4O_9$ ,  $U_3O_8$ , and  $UO_3$ . Uranium dioxide is the most important one because it is used as nuclear fuel in nuclear power plants.  $UO_2$  can have a wide stoichiometric variation due to excess or deficiency of oxygen in its crystal lattice, which can cause significant modifications of its properties. O/U relation determination by gravimetry cannot differentiate a stoichiometric deviation from contents of other uranium oxides in  $UO_2$ . The presence of other oxides in the manufacturing of  $UO_2$  powder or sintered pellets is a critical factor. Fourier Transform Infrared Spectroscopy (FTIR) was used to identify  $U_3O_8$  in samples of  $UO_2$  powder.  $UO_2$  can be identified by bands at  $340\text{ cm}^{-1}$  and  $470\text{ cm}^{-1}$ , and  $U_3O_8$  and  $UO_3$  by bands at  $735\text{ cm}^{-1}$ ,  $910\text{ cm}^{-1}$ , respectively. The methodology for sample preparation for FTIR spectra acquisition is presented, as well as the calibration for quantitative measurement of  $U_3O_8$  in  $UO_2$ . The content of  $U_3O_8$  in partially calcined samples of  $UO_2$  powder was measured by FTIR with good agreement with X-rays diffractometry (XRD).

**Keywords:** FTIR, uranium dioxide, triuranium octoxide.

## 1. Introduction

$UO_2$  is the most used nuclear fuel in nuclear power plants. It is manufactured in the form of sintered cylindrical pellets by powder metallurgy processes. It has been very well studied because it shows changes in its properties due to excess or deficiency of oxygen in wide stoichiometric ranges (O/U relation). O-U system presents various oxides, which have good dimensional stability under radiation and are chemically stable in a nuclear reactor environment.

The stoichiometry is very important for  $UO_2$  performance as nuclear fuel. Fuel oxygen potential and O/U ratio have influ-

ence on mechanisms controlled by diffusion, such as grain growth, creep, release of fission gases, and thermal conductivity, in addition to chemical state and behavior of fission products. The O/U ratio increases with fuel burnup. Moreover, the sintering kinetics of  $UO_2$  pellets is controlled by diffusion processes. Thus, the final characteristics of manufactured  $UO_2$  pellets, which must be kept within very narrow limits, also depend on the O/U ratio of  $UO_2$  powder. The O/U relation is an important parameter to be controlled, both in  $UO_2$  powder and sintered pellets.

The chemical and physical properties of uranium oxides have been studied for many years using various techniques (Guéneau *et al.*, 2002). Small changes in stoichiometry produce considerable variation in uranium oxides, where uranium atoms can be in more than one oxidation state. During  $UO_2$  manufacturing process, both as powder or pellets, all thermodynamically stable phases of O-U system may occur ( $UO_2$ ,  $U_4O_9$ ,  $UO_3$ , and  $U_3O_8$ ). The presence of different phases also changes properties of  $UO_2$  pellets and their thermodynamic performance as nuclear fuel.

Measurement of the O/U ratio is usually performed by gravimetric methods, which give partial information on  $UO_2$  composition. It must be complemented by measures that identify the presence of other phases. X-rays diffraction is usually employed for phase identification and quantification. Nevertheless, it is hard to differentiate the uranium oxide patterns for angles between 20 and 40 degrees, especially at low levels. Thus, the use of X-ray diffraction to control the presence of other phases in  $UO_2$  becomes impractical in an industrial process.

There are indications that infrared spectroscopy is very sensitive to the presence of phases in the O-U system, even at low levels. This technique is little explored for this purpose in the case of O-U system. The objective of this work was to exploit it in order to complement measurements of the O/U ratios. Since this technique is rapid and inexpensive, it has the potential to be used in the line production of  $UO_2$  powder and pellets.

Allen *et al.*, (1976), noticed that infrared spectroscopy may be used to identify phases in O-U system based on bands

observed between 1000 and 200  $cm^{-1}$ . The conclusions of these authors were:

- The  $UO_2$  infrared spectrum has a composite absorption of two components: a transverse optical phonon absorption, TO, at 340  $cm^{-1}$  and a longitudinal optical absorption, LO, which causes a shoulder at 470  $cm^{-1}$ ;

- When oxygen is incorporated into  $UO_2$  crystalline lattice, the intensity TO/LO ratio increases;

- A solid solution of oxygen in  $UO_2$  can be distinguished from a mixture of  $U_4O_9$  and  $UO_2$  by infrared spectroscopy;

- $U_4O_9$  has a weak band at 740  $cm^{-1}$ . This band may be assigned to asymmetric stretching of continuous chains of uranium and oxygen atoms with the same -O-U-O-U- bond length. These strings do not exist in  $UO_2$  fluorite lattice, such that no band is observed in this region.  $\alpha-UO_3$  and  $U_3O_8$ , which contain these chains, have intense bands at 740  $cm^{-1}$ .  $U_4O_9$  has a faint band, possibly due to early formation of these chains.

Axe and Pettit, (1966), measured infrared reflectivity of  $UO_2$  single crystals. They notice a big difference in the region be-

low 700  $cm^{-1}$  compared to spectra obtained with  $UO_2$  powder dispersed in the polymer matrix. This difference was attributed to the effect of dispersion of the infrared beam by particles of  $UO_2$ , which have diameters comparable to the wavelengths of incident infrared radiation.

In order to improve the visualization of  $UO_2$  infrared spectrum, Allen *et al.*, (1976), acquired spectra at 5 K. No improvement was observed, thus showing that the bands are not due to thermodynamic effects. To visualize the band at 500  $cm^{-1}$  of  $U_4O_9$ , Allen and Holmes, (1994), had dispersed 3 parts of oxide in 100 parts of KBr. In other oxides samples the dispersion was 1 part of oxide in 100 parts of KBr. The band at 450  $cm^{-1}$  in  $U_4O_9$  spectrum was attributed to the fact this oxide is the only one to show mixed valences. The bands at 425  $cm^{-1}$  and 510  $cm^{-1}$  were assigned to  $U_3O_7$ , respectively  $\beta-U_3O_7$  and  $\gamma-U_3O_7$ . Ohwada and Soga, (1973), reported a strong band of  $\alpha-U_3O_8$  at 735  $cm^{-1}$ . Hoekstra and Siegel, (1973), attributed this band to possible hydration of the oxide, which would have the kind of deformation U-O-H chain.

## 2. Materials and methods

$UO_2$  powder was provided by IPEN - Institute of Energy and Nuclear Research.  $U_3O_8$  powder was obtained at CDTN by calcining  $UO_2$  powder in air for 3 hours at 400°C. Fourier Transform infrared spectroscopy (FTIR) was performed with a BOMEM spectrometer, model MB102, in the 7000-400  $cm^{-1}$  range with resolution of 8  $cm^{-1}$  and 64 scans, at absorbance mode. Due to the intense absorption of infrared radiation by the uranium oxides, it was nec-

essary to disperse the samples in KBr powder (Sigma Aldrich, spectroscopic grade, 99.99% purity). For a given KBr mass 1% mass of uranium oxide was diluted.

The mixtures of  $UO_2$  and  $U_3O_8$  powders shown in Table 1 were prepared to calibrate the FTIR spectra and to be used as reference for the quantitative analysis with XRD. Figure 1 shows the FTIR spectra of pure  $UO_2$  and pure  $U_3O_8$ . The band at 735  $cm^{-1}$  is related only to  $U_3O_8$ . The intensity

of this band in the spectra of  $UO_2/U_3O_8$  mixtures was used to estimate the content of  $U_3O_8$ . The regression of the calibration curve was performed with Minitab 17.

The XRD diffractograms were obtained with a RIGAKU X-ray diffractometer, model D/MAX-ULTIMA and the quantitative analysis of the  $UO_2$  and  $U_3O_8$  mixtures was carried out considering (001) peak by the RIR (reference intensity ratio) method using JADE 9.0 software.

$UO_2$ (w/o)	99	97	95	93	90	80	60	40	20
$U_3O_8$ (w/o)	1	3	5	7	10	20	40	60	80

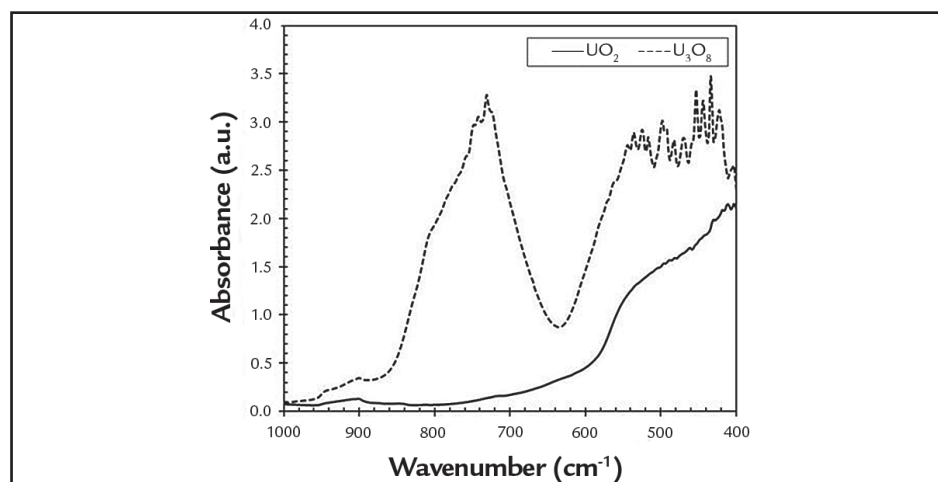


Table 1  
Mixtures of  $UO_2$  and  $U_3O_8$   
used to calibrate the FTIR spectra.

Figure 1  
FTIR spectra of  $UO_2$  and  $U_3O_8$  powder.

To obtain an unknown mixture of  $\text{UO}_2$  and  $\text{U}_3\text{O}_8$  powders, 7.0 g of  $\text{UO}_2$  powder samples were partially calcined in

air at 300, 310, 320, 330 and 340 °C for two hours with a 10 °C/min heating rate in a muffle furnace. The calibrated FTIR

and RIR method using JADE 9.0 software were used to estimate the  $\text{U}_3\text{O}_8$  content in these calcined  $\text{UO}_2$  samples.

### 3. Results and discussion

Table 2 shows values (absolute and relative to 100%  $\text{U}_3\text{O}_8$ ) of intensity of the band at 735  $\text{cm}^{-1}$  of known  $\text{UO}_2$

and  $\text{U}_3\text{O}_8$  mixtures as a function of  $\text{U}_3\text{O}_8$  concentration.

Figure 2 shows the linear regression

correlating  $\text{U}_3\text{O}_8$  content with relative absorbance at 735  $\text{cm}^{-1}$  (confidence level of 95%). The linear model can be expressed by:

$$rel.abs.735 = (0.0494 \pm 0.0089) + (0.0089 \pm 0.0002) \times w/o.U_3O_8 \quad (1)$$

$\text{U}_3\text{O}_8$ w/o	Replica	735 $\text{cm}^{-1}$ band intensity a.u.	735 $\text{cm}^{-1}$ band intensity relative to 100 w/o $\text{U}_3\text{O}_8$	$\text{U}_3\text{O}_8$ w/o	Replica	735 $\text{cm}^{-1}$ band intensity a.u.	735 $\text{cm}^{-1}$ band intensity relative to 100 w/o $\text{U}_3\text{O}_8$
0	1	0.080	0.032	10	1	0.392	0.158
	2	0.078	0.031		2	0.393	0.159
	3	0.078	0.031	20	1	0.638	0.258
	4	0.077	0.031		2	0.633	0.256
1	1	0.141	0.057	40	1	1.038	0.420
	2	0.144	0.058		2	1.040	0.420
3	1	0.169	0.068	60	1	1.439	0.582
	2	0.171	0.069		2	1.440	0.582
5	1	0.230	0.093	80	1	1.685	0.681
	2	0.229	0.093		2	1.686	0.681
7	1	0.326	0.132	100	1	2.474	1.000
	2	0.311	0.126		2	2.475	1.000

Table 2  
Intensity of the band at 735  $\text{cm}^{-1}$  of mixtures of  $\text{UO}_2$  and  $\text{U}_3\text{O}_8$  powders.

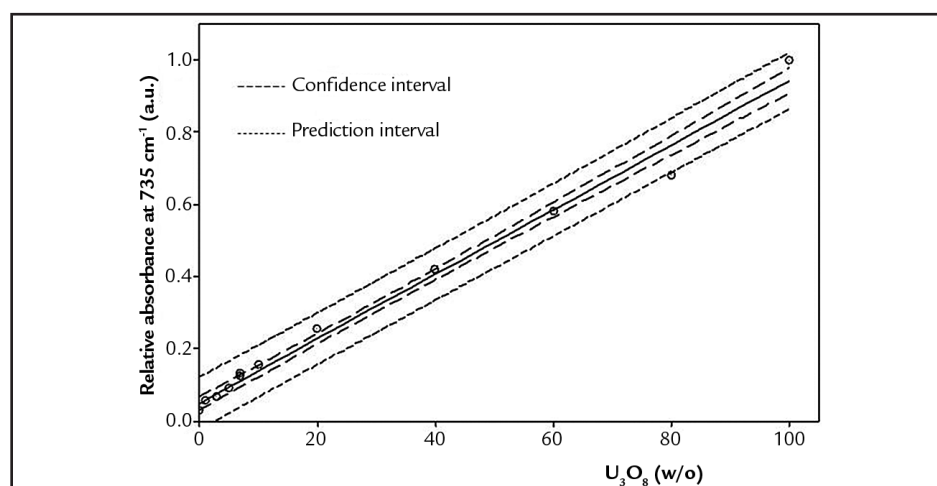


Figure 2  
Linear correlation model for the relative absorbance at 735  $\text{cm}^{-1}$  and the content of  $\text{U}_3\text{O}_8$  ( $\alpha = 0.95$ ).

$\text{U}_3\text{O}_8$  content in partially calcined  $\text{UO}_2$  powder was estimated by FTIR using Equation 1. The results are shown in Table

3 compared with determinations obtained by X-rays diffractometry (DRX). Figure 3 shows that the agreement is quite good.

This method can also be extended to other oxides of the O-U systems, like  $\text{UO}_3$  (band at 910  $\text{cm}^{-1}$ ) or  $\text{U}_4\text{O}_9$ .

Calcining temperature (°C)	Relative absorbance at $735\text{ cm}^{-1}$	Estimated $U_3O_8$ content (w/o)	
		FTIR	DRX
300	0.365	35.46±2.07	43.6
310	0.543	55.46±2.52	57.2
320	0.697	72.76±2.91	80.3
330	0.826	87.26±3.24	93.1
340	0.923	98.16±3.48	99.3

Table 3  
Estimation of  $U_3O_8$  in partially calcined  $UO_2$  powder (FTIR versus DRX).

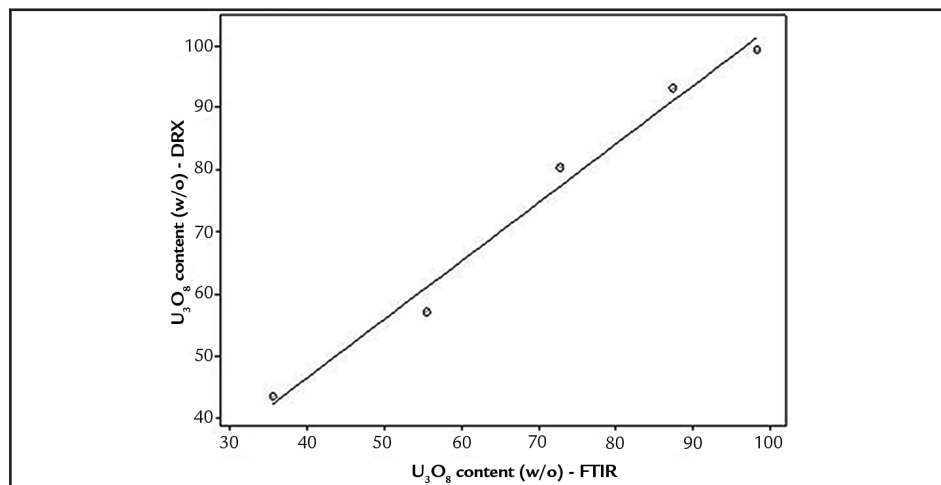


Figure 3  
Comparison of measurement of  $U_3O_8$  concentration in partially calcined  $UO_2$  powder (DRX versus FTIR).

#### 4. Conclusion

Fourier Transform Infrared Spectroscopy (FTIR) was used to measure contents of  $U_3O_8$  in partially calcined  $UO_2$  powders with good agreement with X-rays diffractometry measure-

ments. A methodology for preparing uranium oxide samples for FTIR and XRD measurement was presented. Due to its low cost, simplicity, and rapidity, FTIR may be considered to complement

O/U ratio measurements by gravimetric methods in  $UO_2$  powder and pellet manufacturing. This technique may also be extended to other uranium oxides, like  $UO_3$  or  $U_4O_9$ .

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