



# Fatigue resistance of endodontic instruments manufactured in NiTi CM Wire and in conventional NiTi alloy with electrochemical treatment

Resistência à fadiga de instrumentos endodônticos fabricados em NiTi CM Wire e em niti convencional com tratamento eletroquímico


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## ABSTRACT

### Objective

This study compared the fatigue behavior of endodontic instruments manufactured with conventional NiTi alloy electropolishing, RaCe (FKG Dentaire, LaChauxdeFonds, Switzerland), with instruments manufactured with NiTi CM Wire subjected to thermomechanical treatment, in the manufacturing process, HyFlex CM (Coltene Whaledent, Cuyahoga Falls, Ohio, USA), both with similar geometry and dimensions in order to determine the influence of the manufacturing process in the fatigue resistance.

### Methods

The methodology consisted of twenty HyFlex CM and RaCe instruments with D0 0.25 mm, taper 0.06 mm / mm, 25 mm length, both with triangular cross section. The fracture resistance was evaluated by static fatigue test, using a stainless artificial canal with 5mm of radius (86°), recording the time and calculating the number of cycles until fracture occurs (NCF). For statistical analysis the Student t test was used. The fractured instruments surface was analyzed by SEM.

### Results

The NCF was significantly higher for HyFlex CM instruments in comparison with RaCe files ( $P < 0.05$ ) being 1336% more resistant to fatigue. The analysis of the fractured surface by SEM showed ductile-kind morphological characteristics for both instruments and the absence of plastic deformation.

### Conclusion

HyFlex CM instruments present higher values of NCF. Thus, it can be concluded that the thermal treatment to which these instruments with CM Wire alloy are submitted makes them more resistant to fracture than Race instruments manufactured with conventional NiTi alloy electropolishing.

**Indexing terms:** Endodontics. Nickel. Titanium.

## RESUMO

### Objetivo

Este estudo comparou a vida em fadiga de instrumentos endodônticos fabricados com a liga de NiTi convencional com eletropolimento de superfície, RaCe (FKG Dentaire, LaChauxdeFonds, Suíça), com instrumentos fabricados com a liga de NiTi CM Wire, submetidos a tratamento

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termomecânico, no processo de fabricação, HyFlex CM (Coltene Whaledent, Cuyahoga Falls, Ohio, EUA), ambos com geometria e dimensões semelhantes, visando determinar a influência do processo de fabricação das ligas e do acabamento superficial na resistência à fadiga.

### Métodos

Foram utilizados vinte instrumentos HyFlex CM e RaCe com D0 0,25mm, conicidade 0,06mm/mm, 25mm de comprimento, ambos com seção transversal triangular. A resistência à fratura foi avaliada através de teste estático de fadiga cíclica, utilizando um canal artificial em aço-inoxidável com 5mm de raio (86°), sendo registrado o tempo e calculado o número de ciclos para ocorrer a fratura (NCF). Para análise estatística empregou-se o teste *t* de Student. As superfícies de fratura dos instrumentos foram analisadas em MEV.

### Resultados

O NCF foi significativamente maior para os instrumentos HyFlex CM em comparação com as limas RaCe ( $p < 0,05$ ), sendo 1336% mais resistentes à fadiga. A análise das superfícies fraturadas em MEV revelou características morfológicas do tipo dúctil para ambos os instrumentos e ausência de deformação plástica.

### Conclusão

Os instrumentos HyFlex CM apresentaram valores mais elevados de NCF. Deste modo, pode-se concluir que o tratamento térmico a qual estes instrumentos com a liga CM Wire foram submetidos os torna mais resistentes à fratura do que os instrumentos Race, fabricados com a liga de NiTi convencional com eletropolimento.

**Termos de indexação:** Endodontia. Níquel. Titânio

## INTRODUCTION

The use of automated nickel-titanium (NiTi) instruments has been widespread in endodontic practice due to its shape memory and superelasticity. However, the greatest concern in the use of these instruments has been the fatigue fracture in curved tooth canals [1,2]. By rotating freely in a curvature root canal, the instrument is subjected to alternating tensile and compression stresses on the outer and inner wall of the curve, respectively. These repeated cycles of stress cause cumulative microstructural changes, inducing nucleation and formation of cracks that grow, coalesce and propagate, culminating in fatigue fracture [2-5]. Fatigue resistance is concerned to the number of repeated loads (cycles) that the endodontic instrument will withstand under load until breakage occurs. The number of cycles, which is cumulative and unpredictable, is related to the intensity of the stresses imposed on the instrument and its value is obtained by multiplying the rotational speed by the time to fracture occurs [2-5].

Several factors can influence the mechanical properties of the instruments and, therefore, the resistance to cyclic fatigue. One of these factors are the remaining defects after the machining process, such as grooves and small surface cracks, leading the instrument to fatigue rupture presenting a smaller number of cycles than expected. In order to reduce these defects, some manufacturers have used the surface electropolishing method [6,7].

Recently, new manufacturing technologies with thermomechanical treatments have been developed with the aim of improving the microstructure of the alloys providing instruments with greater flexibility and resistance

to fracture [8-10], such as Hyflex CM® (Coltene Whaledent, Cuyahoga Falls, OH), manufactured with NiTi CM Wire alloy with controlled memory [10].

CM Wire is a new NiTi alloy introduced in Endodontics in 2010 ((DS Dental, Johnson City, TN) undergoing a special thermomechanical treatment which controls the memory of the material, making it extremely flexible, but without the shape memory of conventional Nit files. So far the manufacturing process and the heat treatment to which they are submitted have not been revealed. Hyflex CM® instruments, made with this new alloy, were marketed in 2011 and, according to the manufacturer, are 300% more resistant to fatigue than other instruments available on the market [11,12].

Few studies on the mechanical behavior of NiTi CM Wire instruments in relation to the conventional NiTi instruments with electrochemical treatment are found in the literature. The instruments 25 taper 0.06 are used to make the union of the apical and middle segments in the chemical mechanical preparation of the root canal and provide a conicity that allows an adequate irrigating flow.

The aim of this study was to compare fatigue behavior in the critical region of the instruments manufactured with CM Wire (Hyflex CM - Coltene Whaledent) and with conventional electropolishing NiTi alloys (Race - FKG Dentaire), with nominal diameter 25 and taper 0.06mm/mm.

## METHODS

The present study consisted of twenty NiTi engine-

driven instruments as follows: 10 RaCe files (FKG Dentaire, La Chaux-de-Fonds, Switzerland) and 10 Hyflex CM files (Coltene Whaledent, Cuyahoga Falls, Ohio, United States). The investigated instruments presented a cross section with a triangle shape, D0 diameter of 0.25 mm, taper 0.06 mm / mm and 25 mm of total length.

### Fatigue test

An artificial (Figure 1) stainless steel canal containing 1.4 mm of internal diameter and 19 mm of total length was used. The curved segment, located between two straight segments of 7 and 3 mm, presented 9 mm in length, 86 degrees of curvature and a curve radius of 6 mm as observed in a previous study [13].

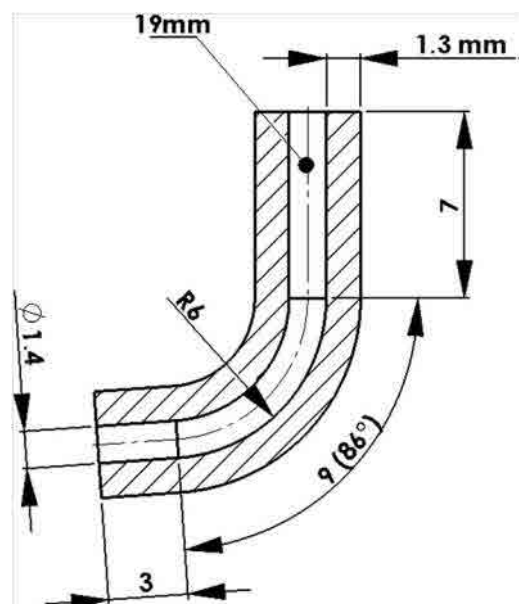


Figure 1. Drawing of the artificial canal used in the cyclic fatigue experiment.

A stainless steel device consisting of a quadrangular base and a vertical axis was used. The vertical axis contained a structure that allowed the fixation and movement of the micromotor / contra-angle. A vise was used, at the base of the device, in order to fix the artificial canal. An opening in the base of the device allowed the vise to move in a horizontal direction, causing, during the insertion of the instrument in the canal, a coincidence of the axes of the instrument with that of the straight part of the canal.

During the test, the canal was filled with glycerin in order to reduce the friction of the instrument against the canal wall and minimize the heat release. Each instrument was positioned in the contra angle / micromotor with speed reduction of 10:01 (VDW Silver, VDW, Munich, Germany) and inserted in the canal until the tip touched a bulkhead located at the end of the curved segment of the canal. This bulkhead was then removed and aimed at standardizing the penetration distance of the instrument within the canal.

Ten RaCe and ten Hyflex CM instruments were clockwise rotated at a speed of 300 rpm until fracture occurred. The time to fracture was considered according to the visual observation, being timed by the same operator, using a digital timer (Technos - Zona Franca de Manaus, Brazil).

The number of cycles for fracture (NCF) was calculated by multiplying the rotation speed by the elapsed time (in seconds) until the fracture of each instrument. The results were submitted to statistical analysis, using Student's t-test, with significance level of 5%.

The fractured surfaces and helical shafts of three instruments of each group were randomly selected and analyzed by scanning electron microscopy (Jeol JSM 5800, Tokyo, Japan) in order to determine the type of fracture and the presence of plastic deformation on the shaft.

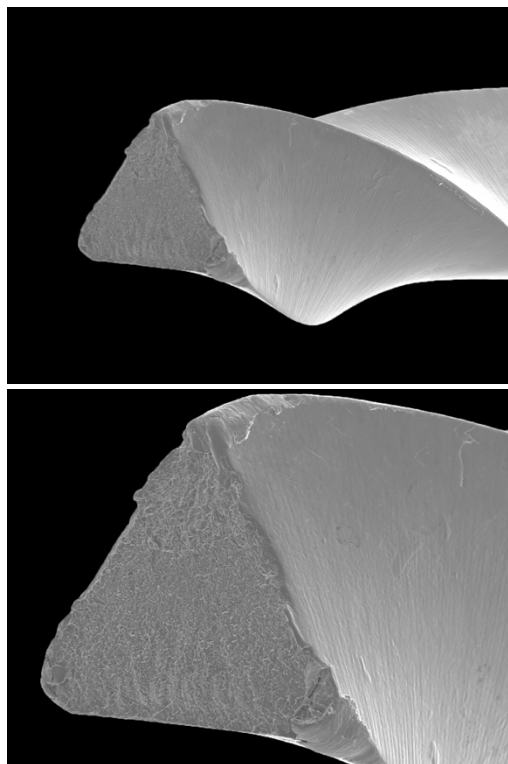
## RESULTS

The time averages for fracture (in seconds) and mean number of cycles for fracture (NCF) are shown in Table 1. The Hyflex CM instruments presented higher fatigue strength than the RaCe instruments ( $p < 0.05$ ).

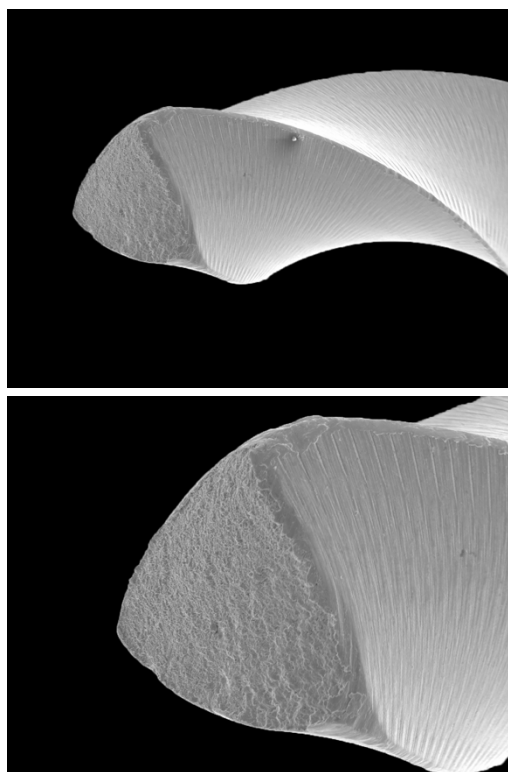
Table 1. Mean ( $\pm$  standard deviation) of Time (seconds) and number of cycles for fracture (NCF) of tested instruments.

	RaCe	Hyflex CM
Time	7.26 ( $\pm$ 1.1635642)	103.418 ( $\pm$ 20.49834)
NCF	36.3 ( $\pm$ 5.812821)	517,1 ( $\pm$ 102.4917)

The scanning electron microscope (SEM), showed that the shafts near the fracture point presented ductile morphological characteristics, showing no plastic deformation of the lateral cutting edges (Figures 2 and 3).



**Figure 2.** SEM analysis of the fractured surface of the Race file revealing absence of plastic deformation in the helical shaft.



**Figure 3.** SEM analysis of the fractured surface of the Hyflex CM file revealing absence of plastic deformation on the helical shaft

## DISCUSSION

In the present study, the results demonstrated that Hyflex CM instruments were 1336% more resistant to cyclic fatigue, presenting a statistically significant difference ( $p < 0.05$ ) in relation to Race instruments. Considering that the instruments of this study presented the same geometric form of the cross-section, same diameter in D0 and same taper, it is probable that the thermomechanical treatment realized in the NiTi CM-Wire may have favorably influenced the mechanical behavior of these new instruments

The metallic canal used in the cyclic fatigue test showed a curvature located at the transition from the apical third to the middle, allowing the analysis of which instrument would better resist fatigue in this area, making the transition between these segments safer. The taper 0.06 was chosen for irrigating substance supply and the diameter of 25 due to its wide clinical use.

Although Race instruments receive electrochemical treatment in order to reduce defects from the manufacturing process that acts as concentrators points of tension aiming at improvement in the mechanical behavior of the same when subjected to loading, electropolishing is intended to reduce surface defects and not the internal defects [14]. Its role in increasing fatigue resistance is considered controversial, with results not always favorable [13,15].

Concerning Hyflex CM instruments, a study on X-ray analysis of dispersive energy showed a lower percentage of nickel weight than the other instruments evaluated. However, thermomechanical history seems to have a much more crucial effect on mechanical strength than composition deviations [16].

Although the thermal treatment produces a better arrangement of the crystalline structure as well as modifications in the percentage of phases of the NiTi alloy, resulting in greater flexibility and better mechanical behavior, no information is given on the temperatures, duration and treatment of Hyflex CM [17]. Patented, manufacturing processes are highly influenced by temperature and time intervals, and every small change makes this manufacturing process unique and exclusive. Therefore, it is not easy to determine whether the improvement in the flexibility of the Hyflex CM instruments is due to either the unique chemical composition, the heat treatment, or both [18].

Comparative studies of endodontic instruments made with Niti CM Wire, M-Wire and conventional

alloys have shown that the CM Wire (Hyflex CM) has greater resistance to fatigue than others, with statistically significant differences [14,19-21]. Although consistent with these results, in the present study the number of fracture cycles (NCF) was lower than that observed in most of the studies [14,20,21], which can be explained by the differences in methodology used.

The fatigue test used in this study was the static test and the artificial canal, although it contained a curvature radius similar to the mentioned manuscripts, presented a longer arc length, besides a severe curve, which variables may have caused the stress increase imposed on the instruments Hyflex CM, decreasing the time for fracture occurrence and consequently the NCF values.

Among the Hyflex CM instruments, it was demonstrated that those with a smaller diameter tip and lower taper showed higher NCF values in canal with 90° and 5mm radius [22], fact expected due to the fatigue fracture be influenced by factors such as morphology and dimensions of canals and instruments [2]. For the reasons mentioned above, the NCF results of the present study were lower than those obtained for instruments of similar size.

Due to standardization lack in the fatigue test methods of endodontic instruments, studies have used different devices and methodologies [23]. Consequently, it is of utmost importance to formulate an international standard for performing the fatigue tests of instruments working in canals, in order to obtain more reliable results.

With regard to the morphological characteristics of the fracture surface it can be fragile, characterized by a smooth, shiny or ductile surface, with presenting hemispheric dimples.

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SEM analysis showed that the instruments of the study groups presented a cross section with the same triangular shape and the fracture surfaces analyzed in both instruments did not show differences in morphological characteristics; the helical shafts of the fractured instruments did not present evidence of plastic deformation; all surfaces presented morphological characteristics with the ductile fracture failure, as observed in previous studies [5,6,13].

## CONCLUSION

Hyflex CM instruments have shown higher NCF values than the Race instruments, representing a safer option for the chemical mechanical preparation of root canal systems that need greater taper in the apical thirds (0.06). Consequently, it can be stated that Hyflex CM instruments, manufactured with the NiTi CM Wire alloy, subjected to thermomechanical treatment are more resistant to fatigue fracture than the RaCe instruments, manufactured with conventional NiTi and electropolishing.

## Collaborators

IFAJ INOJOSA, contributed in the writing phase of the article and statistical analysis. HP LOPES, participated in the implementation of the experimental phase and written review. PLR PEREIRA, participated in the execution of the experimental and written phase. DL NASCIMENTO, participated in the execution of the experimental and written phase. CN ELIAS, participated in the implementation of the experimental phase. VTL VIEIRA, participated in the implementation of the experimental phase and written review. MVB VIEIRA, participated in the implementation of the experimental phase.

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