



# Influence of Abutment Collar Height and Implant Length on Stress Distribution in Single Crowns

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This *in silico* study evaluated the influence of the abutment collar height and implants length on the biomechanical behavior of Morse taper single dental implants with different crown-to-implant ratio. Six virtual models were constructed (S11, M11, L11, S13, M13 and L13) by combining short (S: 2.5 mm), medium (M: 3.5 mm) or long (L: 4.5 mm) abutment collar heights with different implant lengths (11 or 13-mm). An upper central incisor of 11-mm height was constructed on top of each abutment. Each set was positioned in a virtual bone model and exported to analyze mathematically. A 0.60-mm mesh was created after convergence analysis and a 49 N load was applied to the cingulum of the crown at an angle of 45°. Load-generated stress distribution was analyzed in the prosthetic components according to von Mises stress criteria ( $\sigma_M$ ) and in the cortical and cancellous bone by means of shear stress ( $\epsilon_{max}$ ). The use of longer collar abutments (L11) increased the stress on the abutment by 250% and resulted in 40% higher stresses on the screw and 92% higher cortical shear stresses compared to short collared abutments (S11). Increasing the implant length produced a slight stress reduction on cortical bone. Cancellous bone was not affected by the crown-to-implant ratio. Longer abutment collars concentrate stresses at the implant level and cortical bone by increasing the crown-to-implant ratio.

Key Words: dental implants; prosthetic abutments, finite element analysis, single dental implants, anterior single crowns

## Introduction

The distance between the top of marginal peri-implant soft tissue and the implant platform determines the collar height of the prosthetic abutment that is needed for an adequate biological width and emergence profile of the crown (1). To guarantee esthetically pleasing results, abutment selection according to gingival height index depends on two main factors: i) the depth of the gingival sulcus guided by the ocluso-cervical gingival height and ii) the restorative vertical space (2). Patients with deeper gingival sulcus usually need longer abutment collars than patients with shallow ones. The minimum collar abutment height required to guarantee appropriate esthetics should be at least 1 mm below the gingival margin. Although higher abutments would reduce the peri-implant marginal bone loss due to the increased crown to bone distance (3), those abutments also increase the crown-to-implant ratio (C:I) by increasing the collar length, which in turn influences the implant's biomechanical behavior in a way that may increase marginal bone loss.

In a biomechanical scenario, the fulcrum in an implant-supported single crown is located at the implant platform level. Consequently, higher abutments collars increase the lever effect during loading (1-3). Furthermore, assuming the height of abutment from implant platform to the top of abutment, including abutment collar, an increase in the collar height might result in an increase in the vertical

cantilever (1). This phenomenon can be intensified in the anterior region where the set is submitted to oblique loading as a result of chewing (4), especially on abutments connected to Morse taper implants that present a narrow structure at the implant-abutment interface. Previous studies showed that increasing the crown height poses a risk for rehabilitations, as the bone stress increases by about 20% for each mm of increased crown height (5,6).

Using implants with higher length could increase the resistance arm and improve the stress distribution (7,8). According to Rubo et al. (7), increasing implants length from 10 to 13 mm contributes a decrease of about 14% in total stress. Although longer implants do not influence the abutment deflection, they may better dissipate the stresses arising from the masticatory forces and reduce biological and technical complications due to unfavorable C:I ratio (1,9).

To clarify the influence of the abutment collar height on stress distribution, this study evaluates the biomechanical behavior of single Moser taper implants connected to abutments of different collar heights.

## Material and Methods

### Experimental Design

Six three-dimensional models of a single-crown implant-supported restoration were constructed according to implant length (11 or 13-mm) and abutment collar height: short (S,

2.5-mm), medium (M, 3.5-mm) and long (L, 4.5-mm): S11, M11, L11, S13, M13 and L13 respectively. All models were loaded with 49 N at 45° to the cingulum of the crown (10). The data were evaluated using the maximum shear stress ( $\epsilon_{max}$ ) for the cortical and cancellous bone and the von Mises stress ( $\sigma_M$ ) for the implant, abutment and screw.

### Model Construction

The anterior region of an edentulous maxilla was reproduced using SolidWorks 2013® (SolidWorks® Corp, Waltham, MA, USA) based on digital computed tomography images. The bone model was composed of cancellous bone surrounded by 1.5 mm of cortical bone that corresponds to type III bone quality (11). All 3D CAD models in this study were designed to standardize the studied factors (abutment collar height and implant length). The implant was inserted at 1 mm bellow bone level. A single cemented-retained restoration in the maxillary anterior region was simulated, supported by a Morse taper implant (4.1-mm platform) with two different lengths (11 or 13-mm). An anatomic abutment of the central incisor and its respective screw were modeled with different collar length: 2.5 mm (short - S), 3.5 mm (medium - M) and 4.5 mm (large - L). A 11-mm high central incisor crown was reproduced based on human extracted teeth microtomographic images and cemented to the abutment with a 50- $\mu$ m thick layer of resin cement. A representative image of C:I ratios determination and bending moment can be seen in Figure 1, as well as, the 6 models created to be tested. The C:I ratios were calculated by dividing the total crown length (11-mm + abutment collar height) by the respective implant lengths: 1.23, 1.32, 1.41, 1.04, 1.12 and 1.19 for the S11, M11, L11, S13, M13, and L13 models, respectively. The models were exported to Ansys Workbench 14.0 FEA software (Swanson Analysis Systems, Inc. Houston, PA, USA) to perform the numerical analysis.

### Numeric Analysis

The mesh was achieved using a 0.6 mm tetrahedral elements configuration defined after a 5% tolerance convergence analysis. The material properties of implants, abutments and screws were assumed to be as titanium. On the other hand, the prosthetic crown was considered as ceramic (lithium disilicate) cement-retained by a resin luting cement. The Young's modulus and Poison ratio used were listed in the Table 1 (12-14). The implant was inserted at 1 mm bellow bone level according to manufactures instruction. All materials were considered homogenous, isotropic and linearly elastic.

The boundary conditions were defined by fixing both lateral exterior surfaces of the bone segment. A load of 49 N was applied in the palatal region of the prosthetic

crown angulated at 45° with the long-axis of the implant (10). The values of maximum shear stress ( $\epsilon_{max}$ ) for cortical and cancellous bone and von Mises stress ( $\sigma_M$ ) for implants and prosthetic components were obtained. The difference percentage were calculated and compared among the models.

## Results

The maximum shear stress for cortical and cancellous bone and maximum von Mises stress for the implant and prosthetic components are described in Table 2. The percentage differences in function of the abutment's collar length and implant length are described in Table 3. For the 11 mm implant, a higher C:I ratio (S11→L11) increased the stress in the abutment, screw, implant and cortical bone. The prosthetic abutments were the most impaired piece of the joint, and the longest abutments showed an increase of 250% compared to the shortest ones (Small: 204-MPa; Long: 712-MPa). Higher implant lengths (13 mm) resulted in a negligible stress decrease in the abutments (-2%).

Longer abutments recorded 40% higher stresses in the screw compared to short abutments for both implants length (S11 and S13: 99-MPa; L11 and L13: 139-MPa). The shear stress at cortical bone was higher when the longer abutment was used, increasing 75% in the case of the 11-mm implant (S11→L11) and 92% when the 13-mm implant was used (S13→L13). The cortical bone was negative affected by the higher C:I ratio for both implant sizes. Cancellous bone was not affected by the crown-to-implant ratio. Qualitative stress distribution patterns and maximum peak concentration at the regions of interest are shown in Figure 2.

## Discussion

The C:I ratio can be responsible for biological or mechanical damage, as the stress tolerance limits are still not accurately known. This study evaluated the combined influence of abutment height and implant length on the biomechanical behavior of single-implants during restoration. Therefore, three-dimensional finite element analysis was used to predict the biomechanical

Table 1. Material properties used for the numerical simulation

Material	Young's modulus (GPa)	Poison ratio	Reference
Cortical bone	13.6	0.26	(12)
Cancellous bone	1.36	0.31	(12)
Ti-6Al-4V	110	0.35	(12)
Lithium disilicate	96	0.23	(13)
Resin luting cement	18.3	0.30	(14)

behavior of single dental implants with various dimensions during rehabilitation. The models were assumed to be homogeneous, isotropic, and linearly elastic. The bone and prosthetic crown were constructed based on tomography images and the implant, abutment, and screw were based on commercially available pieces that contribute to improve the accuracy of the models. In addition, a surrounding bone was constructed as an independent piece in order to obtain the specific stress of the peri-implant bone.

The obtained results indicated that the abutment was the most impaired part of the implant during restoration, especially for a high C:I ratio of 1.41. The stress increased by about 250% when a higher collar abutment (4.5 mm)

was associated with an 11-mm implant (L11). These results corroborate those of Machado et al. (15), who observed the predominance of abutment failure in vitro for Morse taper implants that can be attributed to the large contact area between implants and abutments. The reliability of the set is challenged by the thick cervical abutments wall bended to implants platform during oblique loading (1516). Furthermore, a recent systematic review (17) proposed that a C:I ratio higher than 1.46 can be related to prosthetic failure and represents a risk of abutment fracture.

The prosthetic's screws were negatively affected by higher C:I ratios, with stress increases up to 40%, regardless of the implant length. Screw loosening is considered the most important reason for prosthetic failure during rehabilitation, especially for the external hexagon connections (18,19). In cases using internal connections, these failures are more associated with two-piece abutments than solid abutments because they bolt/boltare thicker, with less material that can dissipate the strain energy from the loading during chewing. A systematic review by Gracis et al. (20) pointed out interesting clinical outcomes that can be analyzed during the abutment selection to assess its failure potential: i) the incidence of fracture of metal-based and zirconia-based abutments and that of abutment

screws does not seem to be influenced by the type of connection; ii) loosening of abutment screws was still the most frequently occurring technical complication and seemed to be influenced by the type of connection, more loose screws were reported for externally connected implant systems; iii) proper preload may decrease the incidence of such a complication.

The relationship between occlusal forces on oral implants and the surrounding bone can be compromised by overloading resulting in biological complications or even osseointegration failure (21). The response to an increased mechanical stress below a certain threshold will be a strengthening of the bone by increasing the bone density or apposition of

Table 2. Equivalent von Mises stresses for prosthetic components and implants (MPa) and maximum shear stresses for cortical and cancellous bone (MPa)

	S <sub>11</sub>	M <sub>11</sub>	L <sub>11</sub>	S <sub>13</sub>	M <sub>13</sub>	L <sub>13</sub>
Screw	99.14	109.98	138.59	99.00	109.74	138.70
Implant	179.51	217.79	230.95	180.15	222.92	206.64
Abutment	203.71	293.67	711.99	203.55	297.12	697.98
Cortical bone	22.79	24.15	39.93	19.35	22.89	37.24
Cancellous bone	3.12	2.79	3.42	2.98	3.3	3.41

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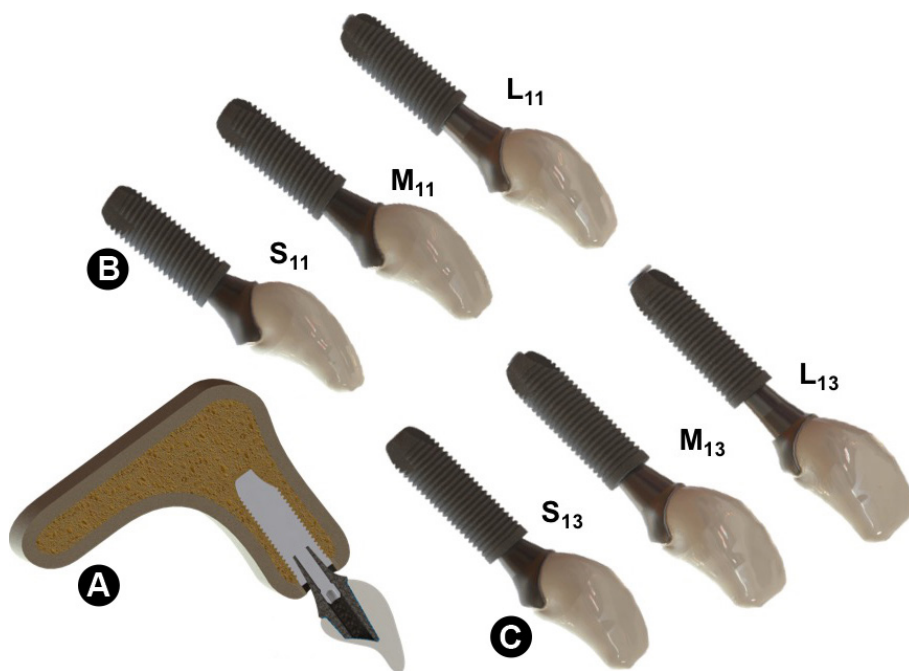


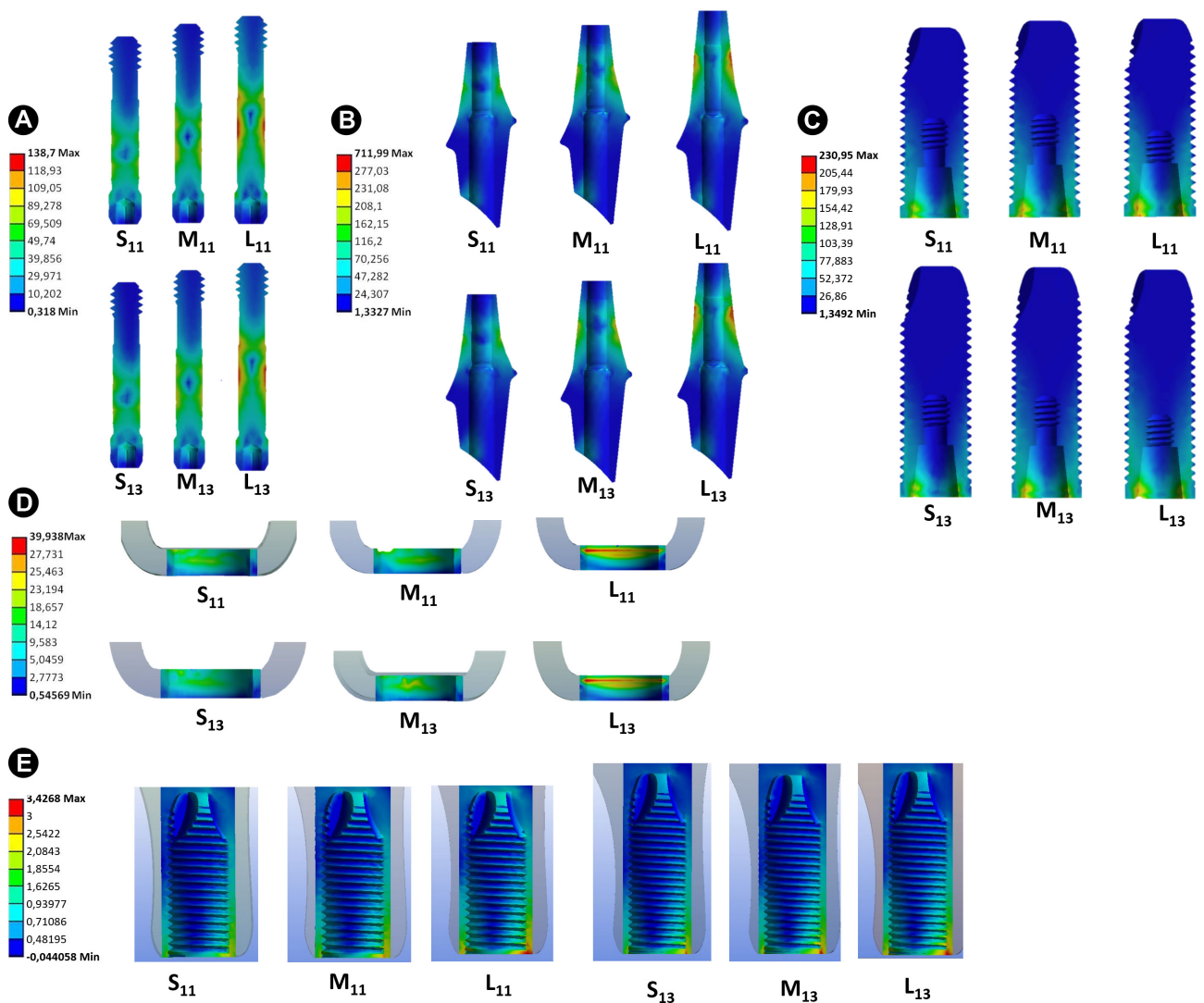
Figure 1. A) Anterior region of edentulous maxilla reproduced using SolidWorks 2013® (SolidWorks® Corp, Waltham, MA, USA) based on digital computed tomography images. Models composition according to the abutments collar height showing the Crown:Implant ratio in the 11-mm (B) the 13-mm (C) dental implants.

bone. On the other hand, fatigue micro-damage resulting in bone resorption may be the result of mechanical stress beyond this threshold (22). The highest cortical shear stresses of 39.93 MPa were observed in the L11 models.

The latter is 75% higher than the corresponding stresses in the S11 models. The region with the maximum peak stress was restricted to the peri-implant bone around the first implant threads. This corroborates the results from

Table 3. Relative stress differences (%) in function of abutment height (Small, Medium and Long) and implant length (11 and 13-mm)

Regions of interest	Difference between abutment heights (%)						Difference between implant lengths (%)		
	M <sub>11</sub> - S <sub>11</sub>	L <sub>11</sub> - M <sub>11</sub>	L <sub>11</sub> - S <sub>11</sub>	M <sub>13</sub> - S <sub>13</sub>	L <sub>13</sub> - M <sub>13</sub>	L <sub>13</sub> - S <sub>13</sub>	S <sub>13</sub> - S <sub>11</sub>	M <sub>13</sub> - M <sub>11</sub>	L <sub>13</sub> - L <sub>11</sub>
Screw	11%	26%	40%	11%	26%	40%	0%	0%	0%
Implant	21%	6%	29%	24%	-7%	15%	0%	2%	-11%
Abutment	44%	142%	250%	46%	135%	243%	0%	1%	-2%
Cortical bone	6%	65%	75%	18%	63%	92%	-15%	-5%	-7%
Cancellous bone	-11%	23%	10%	11%	3%	14%	-5.5	18%	0%



Abutment collar height and implant biomechanics

Figure 2. Maximum stress concentration at the regions of interest for all experimental groups. A: Screws. B: Abutments. C: Implants. D: Cortical bone. E: Cancellous bone.

Rieger et al. (23), who demonstrated that high stress levels induced during bending are concentrated around the neck and are dissipated via the apex.

To test whether the biomechanical behavior could be further improved, longer implants of 13 mm were selected. However, a stress reduction of only 15% in the cortical bone was observed, indicating that higher implants lengths are not able to decrease the stress significantly. Recent studies suggested that implant diameter should be more important than the implants length to control bone overloading since wide implants have a larger bone-implant contact, especially in the cervical region, the stress is concentrated near the first implant's threads in contact with cortical bone (11,24,25). The bone stresses obtained in this study were below the physiologic limits described in the literature for the elastic limit of the human cortical bone (60 MPa) (26). However, it is until unclear the correlation between bone adaptive capacity to distribute stress without biological damages (27), since experimental studies have shown different biomechanical behaviors when oblique forces are involved leading an increased bone response (15,17,26).

Although, a recent study (28) suggested that shorter abutment height is associated with greater marginal bone loss in cement-retained prostheses, our *in silico* study prosthetic abutments with shorter collar heights showed a better biomechanical behavior for all prosthetic components and cortical bone, irrespective of the implant height. Shorter abutments allow to select abutments with increased body height, increasing the crown retention and improving the stability of the crown-abutment-implant connection and the accessibility during impression procedures (1,20). Moreover, implants with higher C:I ratios positively affect the peri-implant marginal bone level (MBL): within the C:I range of 0.6 - 2.36, higher C:I ratios negatively correlate with the peri-implant MBL (9). Clinically, these implants can still achieve good short- to medium-term survival rates, as long as the occlusion and parafunctional habits are controlled (3,9,29). In addition, the placement of platform-switched implants and the use of long abutments connecting cemented crowns to implants would provide greater height for biologic width reestablishment, allow easier removal of excess cement from soft tissue and reducing bacteria-induced inflammation, consequently preventing progression of marginal bone loss in cement-retained restorations (28).

More studies are still required to investigate the stiffness of the system to provide a displacement map of the different structures. This would be needed to fully characterize the potential deformation of the implant-abutment system. Different experimental parameters can also be considered in future modeling studies, such as bone type, positions in the arch, partial and full arch bridge

prostheses, prosthetic connections and loading directions. Higher crown-to-implant ratios in long-collar abutments can negatively affect the biomechanical behavior of single crowns supported by morse taper implants, and the highest stresses are located in the prosthetic abutment. Increasing the crown length has a small positive effect on the cortical bone stress values. The stress in the cancellous bone showed no relation with C:I ratios or implant lengths.

## Resumo

Este estudo avaliou a influência da altura da porção transmucosa do pilar protético com junção cone morse e do comprimento dos implantes no comportamento biomecânico coroas unitárias com diferentes proporção coroa-implante. Seis modelos virtuais (S11, M11, L11, S13, M13 e L13) foram construídos combinando pilares protéticos com transmucoso considerado: curto (S: 2,5 mm), médio (M: 3,5 mm) ou longo (L: 4,5 mm) com diferentes comprimentos de implantes (11 ou 13 mm). Um incisivo central superior de 11 mm de altura foi construído para cada pilar. Cada conjunto foi posicionado em um modelo de osso virtual e exportado para análise matemática. Uma malha de 0,60 mm foi criada após análise de convergência e uma carga de 49 N foi aplicada ao cingulo da coroa em um ângulo de 45°. A distribuição de estresse gerada por carga foi analisada nos componentes protéticos de acordo com o critério de tensão de von Mises ( $\sigma_M$ ) e no osso cortical e medular por meio da tensão de cisalhamento ( $\epsilon_{max}$ ). O uso de pilares com porção transmucosa mais longa (L11) aumentou a tensão no pilar protético em 250%, e resultou em tensões 40% maiores no parafuso e 92% no osso cortical em relação aos pilares com transmucoso curto (S11). O aumento do comprimento do implante produziu uma ligeira redução da tensão de cisalhamento no osso cortical. O osso medular não foi afetado pela relação coroa-implante. Pilares protéticos com porção transmucosa mais longa concentram tensões no implante e no osso cortical, quando a proporção coroa-implante é aumentada.

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