

# PRODUCTION OF LACTIC ACID FROM GLYCEROL BY APPLYING AN ALKALINE HYDROTHERMAL PROCESS USING HOMOGENEOUS CATALYSTS AND HIGH GLYCEROL CONCENTRATION

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**Abstract** - The production of lactic acid from glycerol by means of the alkaline hydrothermal process was evaluated using high concentrations of glycerol. The operating conditions that influence the hydrothermal process were studied. Temperature (250 - 280 °C), catalyst to glycerol molar ratio (0.05 to 0.15), and water to glycerol volumetric ratio (0.8 to 1.5) were evaluated, as well as the use of NaOH and KOH as catalysts. A concentration of lactic acid of 122 g/L was obtained at 260 °C, 0.04 NaOH to glycerol molar ratio, 1.0 water to glycerol volumetric ratio and 3 h of reaction using crude glycerol as raw material. The results showed higher lactic acid concentration and productivity than the fermentative process and the hydrothermal process carried out using low initial glycerol concentration.

**Keywords:** Glycerol; Lactic acid; Hydrothermal processing; Homogeneous catalyst.

## INTRODUCTION

The use and development of renewable energy sources is growing. Biodiesel, one of the alternatives to petroleum-derived diesel fuels, has been developed and is being produced in large industrial scale in several countries. As the production of biodiesel grows, the production of its main by-product (glycerol) also grows. The production of 10 tons of biodiesel generates about 1 ton of glycerol (~10 wt%), which has begun to be considered an unwanted by-product since it cannot be simply dumped into rivers or landfills (Dasari *et al.*, 2005). In recent years, the availability of glycerol increased and new markets and uses for glycerol are required and desired.

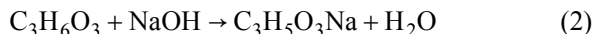
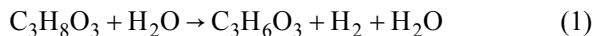
Lactic acid is one of the products that can be obtained from glycerol. Currently, it is used as a precursor for green solvents such as ethyl lactate and in the synthesis of poly(lactic acid), which is a biodegradable polymer. Lactic acid has many applications in the food, textile, leather, cosmetic, chemical and pharmaceutical industries (Ramírez-López *et al.*, 2011).

More than 90% of the lactic acid is produced by fermentation of carbon sources, especially sugars and alcohols (He *et al.*, 2008). The fermentative process has a high selectivity towards lactic acid, but the concentration of lactic acid at the end of the fermentation can be considered low (approximately 50 g/L). Only a few strains of lactic bacteria provides high

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concentrations of lactic acid (approximately 100 g/L) (Budhavaram and Fan, 2009; Gullon *et al.*, 2008; Marques *et al.*, 2008; Nancib *et al.*, 2009).

Glycerol can be converted into lactic acid and other products by hydrothermal processes (Savage, 1999; Shen *et al.*, 2009). The hydrothermal process can be carried out by an alkaline process using a hydroxide as catalyst (usually NaOH or KOH) or by heterogeneous catalysis using a wide range of oxides as catalyst (Ca, Cu, Ni, Au, Zn oxides) (Chen *et al.*, 2014; Hu *et al.*, 2012; Purushothaman *et al.*, 2014; Roy *et al.*, 2011; Xu *et al.*, 2013). In this work, we have focused on the alkaline hydrothermal process to produce lactic acid. The conversion of glycerol to lactic acid (or its lactate) by the alkaline process proceeds through the reactions:



Several studies have reported high yields of lactic acid (> 90%) from many carbon sources (glycerol, sorbitol, mannitol) (Kishida *et al.*, 2005; Ramírez-López *et al.*, 2010; Shen *et al.*, 2009; Zhou *et al.*, 2010). These studies, however, started from low concentrations of the carbon source (< 0.05 v/v). Under this condition, the final concentrations of lactic acid and the productivities of the process are much lower than the concentrations and productivities observed in the fermentative process. To compete with the fermentative process, the hydrothermal process needs to be equivalent or better than the fermentative process.

In this work, the hydrothermal process to produce lactic acid from glycerol was evaluated using high initial concentrations of glycerol (> 0.8 v/v), aiming at an increase in productivity. The main process variables (temperature, catalyst/glycerol mass ratio and water/glycerin volumetric ratio) were studied and their influences on yield and productivity were evaluated.

## MATERIALS AND METHODS

### Materials

All reagents were obtained from Synth (Brazil). Crude glycerol derived from biodiesel production was provided by Petrobras Biocombustível (Quixadá - CE, Brazil).

### Hydrothermal Reaction

The chemical reaction was carried out in a 400 mL batch autoclave reactor (Metalquim, Brazil) made of stainless steel, equipped with temperature and pressure control and a magnetic stirrer. The reactions were carried out by adding glycerol, water and catalyst (sodium or potassium hydroxide) to the reactor, according to the ratios presented in Tables 1, 3 and 4. The volume of reagents in the reactor was always set to 200 mL and the stirrer speed was set at 800 rpm. The reactor was closed and heating began after adding the reagents. Reaction time was set to 3 h after reaching the final reaction temperature (about 20 min after heating started). After 3 h, the reactor was rapidly cooled by passing a cold-water stream (23 °C) through the reactor jacket.

The NaOH to glycerol molar ratios presented in Tables 1, 3 and 4 correspond to the same concentration range of NaOH in the reactor. The difference in numerical value is due to the higher amount of glycerol that was added to each reaction.

### Chemical Analysis

Lactic acid was converted into methyl lactate prior to GC analysis, for better analysis of the results because GC-FID has very poor sensitivity for lactic acid. Derivatization was carried out by mixing 10 mL of reaction mixture with 25 mL of methanol and 6 drops of H<sub>2</sub>SO<sub>4</sub>. The derivatization reaction was carried out overnight at ambient temperature. The calculation of methyl lactate concentration was based on a five point calibration curve constructed using methyl lactate analytical standard (85%) as reference. The derivatization carried out to quantify lactic acid also quantifies the lactate salts because, when sulfuric acid is added to the sample, any lactate salt will be transformed into lactic acid, which is then esterified into methyl lactate. Thus, the formation of lactate salts will be accounted for and expressed as lactic acid.

The samples were analyzed by GC-FID (Thermos model Ultra) using an OV-1 capillary column 30 m in length with 0.25 mm inner diameter and 0.25 μm film thickness. The injector temperature was set at 250 °C. Oven temperature started at 50 °C and was increased to 150 °C at a rate of 5 °C/min and held for 2 min.

Glycerol content was analyzed by FTIR (Agilent model Cary 630). An amount of 300 μL of sample was directly analyzed in the ATR module of the FTIR equipment. The spectral resolution was 4 cm<sup>-1</sup> and 32 scans were accumulated for each spectrum. A

spectral range between 800 and 400  $\text{cm}^{-1}$  was measured. The values obtained at 1420  $\text{cm}^{-1}$  were recorded and used to calculate the concentration of glycerol in the sample. The calculation of glycerol concentration was based on a five point calibration curve constructed using glycerol solutions in distilled water.

The conversion of glycerol was calculated with Equation (3),

$$X = \frac{n_G^0 - n_G}{n_G^0} \quad (3)$$

where  $n_G^0$  is the initial number of mols of glycerol,  $n_G$  is the number of mols of glycerol obtained after the analysis of the sample, and  $X$  is the conversion of glycerol.

By-products and trace elements were analyzed by GCMS (Thermos model ISQ) under the same conditions used for GC analysis (column, injector temperature and oven programming).

## RESULTS AND DISCUSSION

Experiments with low initial concentration of glycerol were carried out as a basis for comparison between the hydrothermal processes using high and low initial concentrations of glycerol. The yields of conversion of glycerol into lactic acid under these conditions are presented in Table 1. The results showed yields up to 76.4%.

Glyceraldehyde, propionaldehyde and gluconic acid were formed during the reaction, but in minor amounts. The conversion of glycerol into these other by-products was between 0.5 and 3%. Propionaldehyde was the main by-product at the lowest temperature (240 °C) and glyceraldehyde was the main by-product at the highest temperature (260 °C).

Table 2 presents the analysis of perturbation of the factors for the hydrothermal process carried out at low glycerin to water molar ratio. The process was mainly influenced by temperature and NaOH to glycerol molar ratio. Higher temperatures and lower NaOH to glycerol molar ratios resulted in higher yields of lactic acid. The statistical analysis indicated that the catalyst to glycerol molar ratio was the main factor influencing the reaction; presenting a negative effect on the hydrothermal process (an increase in the NaOH to glycerol molar ratios produced a decrease in yield).

According to Ramirez *et al.* (2011), the decrease in yield at excess hydroxide ion concentrations is caused by the scission of glycerol at different C–C bonds, resulting in an increasing number of competing reactions, which include the reactions of decomposition of lactic acid, decomposition of reaction intermediates, and the activation of conversion routes of pyruvaldehyde and formate.

The results obtained herein were lower than those reported by Shen *et al.* (2009), who obtained yields up to 90% from the same initial water, glycerol and NaOH concentrations, but under a more severe operating condition (300 °C and 90 bar). The difference in the results shows the importance of operating at higher temperatures if higher yields are desired. A comparison between the results reported herein and by Shen *et al.* (2009) shows a change in the behavior of the reaction regarding the NaOH/glycerol molar ratios. Table 1 shows that the yield decreased with increasing NaOH/glycerol ratios, while Shen's results show the opposite behavior (yield increasing with increasing NaOH/glycerol ratios). The different behavior that was observed may be related to a thermal effect, which may increase the rate of reaction more at high NaOH/glycerol ratios than at low NaOH/glycerol ratios, leading to the differences in behavior found between the studies.

**Table 1: Yield and lactic acid productivity for the hydrothermal treatment of glycerol carried out at low initial glycerol concentration.**

Run	Temperature (°C)	Water to Glycerol volumetric ratio (v/v)	NaOH to Glycerol molar ratio (mol/mol)	Yield (%)	Lactic Acid Concentration (g/L)	Lactic Acid Productivity (g/L.h)
1	247	31.0	0.44	67.6	26.0	8.7
2	250	31.0	0.44	76.4	29.4	9.8
3	240	27.0	0.44	51.1	22.5	7.5
4	250	31.0	0.73	51.3	19.7	6.6
5	252	31.0	0.73	53.4	20.5	6.8
6	245	27.0	0.73	50.2	22.1	7.4
7	241	31.0	1.02	47.1	18.1	6.0
8	244	31.0	1.02	50.2	19.3	6.4
9	240	27.0	1.02	43.4	19.1	6.4

**Table 2: Analysis of perturbation of the factors on the yield of lactic acid for the hydrothermal process carried out at low and at high glycerol concentration\*.**

Factor	Effect	p Value
<b>Hydrothermal process carried out with low glycerol concentration</b>		
<b>Mean</b>	50.13 ± 2.00	0.0001
<b>T</b>	14.41 ± 3.81	0.0325
<b>T<sup>2</sup></b>	- 8.55 ± 4.16	0.1317
<b>Cat</b>	- 17.24 ± 3.34	0.0141
<b>Cat<sup>2</sup></b>	18.19 ± 5.56	0.0467
<b>T x Cat</b>	- 11.27 ± 4.55	0.0895
<b>Hydrothermal process carried out with high glycerol concentration</b>		
<b>Mean</b>	7.20 ± 1.71	0.0040
<b>T</b>	3.17 ± 5.18	0.5586
<b>Cat</b>	- 6.01 ± 2.15	0.0268
<b>T x Cat</b>	0.50 ± 2.70	0.8579

\*Variables in bold represent significant influence at 90% of significance. T – temperature; Cat – catalyst to glycerol molar ratio.

Lactic acid concentration and productivity obtained by Shen *et al.* (2009) were 26.7 g/L and 8.9 g/L.h, respectively. In our research, higher lactic acid concentrations and productivity were obtained (Run 2, Table 1). As such, it is possible to achieve higher productivity under less severe operating conditions, especially under lower temperature and, thus, with lower energy consumption.

Typical fermentation processes for lactic acid production output lactic acid concentrations between 50 to 60 g/L and productivities between 1.0 to 5.0 g/L.h (Guilherme *et al.*, 2011; Oliveira *et al.*, 2009; Silveira *et al.*, 2010). For example, the production of lactic acid employing molasses from hydrolyzed sugarcane fermented by *Lactobacillus casei* presented a maximum concentration of lactic acid of 58.9 g/L and a maximum yield of 1.2 g/L.h (Oliveira

*et al.*, 2009). The production of lactic acid employing cashew apple juice fermented by *Lactobacillus casei* presented a maximum concentration of lactic acid of 59.3 g/L, yields up to 96% and a maximum productivity of 1.7 g/L.h (Guilherme *et al.*, 2011). Gullon *et al.* (2008) obtained productivities as high as 5.1 g/L.h with a lactic acid concentration of 32.5 g/L fermenting apple pomace. High productivities (between 19 and 22 g/L.h) and concentrations up to 38 g/L were reported by (Schepers *et al.*, 2006) fermenting whey permeate and yeast extract using *Lactobacillus helveticus* to produce lactic acid. Higher productivities than the hydrothermal process carried out with low glycerol concentration were also reported by Plessas *et al.* (2008) and by Coelho *et al.* (2011).

Although high yields can be obtained by the hydrothermal process, the concentration of lactic acid in the reaction medium was low when compared to the fermentative process for lactic acid production. An option to increase the concentration of lactic acid in the reaction medium and the productivity of the process would be to increase the amount of glycerol fed to the reactor. Table 3 presents the results obtained for the hydrothermal process operating at high glycerol concentration.

Increasing the amount of glycerol in the reaction mixture decreased significantly the yield of glycerol conversion into lactic acid, but increased the productivity. The yields observed in the process were low and the best condition gave a yield of 19.9%. The process was mainly influenced by the NaOH to glycerol molar ratios, with low NaOH to glycerol molar ratios resulting in higher yields of lactic acid. At high glycerol concentration, the influence of temperature was lower. Statistical analysis also corroborates these observations (Table 2).

**Table 3: Yield and lactic acid productivity for the hydrothermal treatment of glycerol carried out at high glycerol concentration.**

Run	Temperature (°C)	Water to Glycerol volumetric ratio (v/v)	NaOH to Glycerol molar ratio (mol/mol)	Yield (%)	Lactic Acid Concentration (g/L)	Lactic Acid Productivity (g/L.h)
10	260	1.0	0.04	19.9	122.5	40.8
11	260	1.0	0.07	6.9	42.2	14.1
12	260	1.0	0.11	2.3	13.9	4.6
13	270	1.0	0.07	1.8	11.2	3.7
14	270	1.0	0.11	10.3	63.4	21.1
15	280	1.0	0.04	17.7	109.2	36.4
16	280	1.0	0.07	17.2	105.9	35.3
17	280	1.0	0.11	2.1	13.0	4.3
18	270	0.8	0.07	6.2	42.5	14.2
19	270	1.3	0.09	6.0	32.9	11.0
20	270	1.7	0.12	5.0	22.9	7.6

The most significant variable for the process was the concentration of hydroxide, having a negative effect on the yield of lactic acid (lower concentrations of NaOH resulted in higher yields). Temperature and water to glycerol volumetric ratio were not statistically significant for the process at high glycerol concentrations and water to glycerol volumetric ratios ranging from 0.8 to 1.3. Temperatures ranging from 260 to 280 °C are required for the reaction, but the lower levels of temperature should be considered to run the hydrothermal process, since an increase in temperature did not change significantly the yield.

Although a decrease in yield was observed, a significant improvement in lactic acid productivity and concentration in the reaction media was obtained. The productivity of the process increased by 300% for the production of lactic acid, which is a considerable amount. The productivity of the hydrothermal process, under these conditions, was comparable to the productivity and lactic acid concentrations obtained by the best fermentative processes.

The yields and productivity of the process carried out with analytical grade and with crude glycerol were similar, with analytical grade glycerol resulting in a yield 2% higher than when operating with crude glycerol. From an economical point-of-view, it is not required to refine the crude glycerol before using it in the alkaline hydrothermal process. Only filtering would be required to remove suspended materials.

Table 4 presents the experiments carried out using KOH as catalyst. The yield and productivity obtained were, in most cases, lower than when using NaOH as catalyst. Shen *et al.* (2009) reported that the performance of the process when using KOH was superior to NaOH as a catalyst. However, the results obtained herein showed a different trend. The results show that KOH might be preferred when working at higher temperatures and higher water to glycerol volumetric

ratio, while NaOH might be preferred when working at lower temperatures and lower water to glycerol volumetric ratio.

Longer reaction times did not contribute to a higher conversion. The reaction reached an equilibrium after 3 hours and no improvement in yield was observed. Thus, there is no need to spend more time and energy after 3 hours of reaction, since no increase in the conversion of glycerol into lactic acid will be attained.

The production of lactic acid through the hydrothermal process results in the formation of a racemic mixture of L-lactic acid and D-lactic acid. The racemic mixture can be used to produce several chemicals, such as ethyl lactate, propylene glycol, propylene oxide, acrylic acid and other green-labelled chemicals. The use of the racemic mixture in the production of poly(lactic acid) provides a polymer with a low degree of crystallinity and low tensile strength. The pure L-isomer is preferred to produce poly(lactic acid) because it provides a polymer with higher tensile strength and crystallinity and, in this case, the product derived from the fermentative process is preferred (Van Wouwe *et al.*, 2013). The racemic mixture, however, has been added to the pure L-isomer during polymerization to change the properties of poly(lactic acid), producing a wide range of physical properties (Datta and Henry, 2006).

One of the advantages of the fermentative process for the production of lactic acid is the possibility to start with several sources, such as sucrose, glucose, mannitol, fruit residues, glycerol and other sources (Gao *et al.*, 2006; Göksungur *et al.*, 2005; Marques *et al.*, 2008; Silveira *et al.*, 2010; Zhang and Vadlani, 2013). The hydrothermal process, in this sense, is limited to the use of glycerol, and its production should be linked to processes that generate large quantities of glycerol.

**Table 4: Yield and lactic acid productivity for the hydrothermal treatment of glycerol carried out at high initial glycerol concentration using potassium hydroxide as catalyst.**

Run	Temperature (°C)	Water to Glycerol volumetric ratio (v/v)	KOH to Glycerol molar ratio (mol/mol)	Yield (%)	Lactic Acid Concentration (g/L)	Lactic Acid Productivity (g/L.h)
21	250	1.3	0.07	0.4	2.4	0.8
22	260	0.8	0.04	2.6	18.1	6.0
23	260	1.3	0.07	5.9	32.6	10.9
24	260	1.0	0.06	1.4	8.4	2.8
25	245	0.8	0.01	1.0	6.6	2.2
26	250	0.8	0.01	6.2	42.2	14.1
27	250	1.3	0.04	3.2	17.5	5.8
28	255	0.8	0.03	2.6	18.1	6.0
29	255	0.8	0.04	2.6	18.1	6.0
30	250	1.3	0.05	25.1	137.3	45.8

Nowadays, biodiesel plants are the main sources of glycerol and produce large quantities of this chemical. The availability of glycerol at low prices can boost the production of lactic acid by the hydrothermal process.

The atom efficiency of the hydrothermal process is very high (97.8%), which is a positive feature of this process. The fermentative process has a lower atom efficiency (78.9%) since fermentation of sucrose yields lactic acid, but also acetic acid and carbon dioxide.

Thermodynamic data show that the hydrothermal reaction pathway requires 5.6 kJ/mol of lactic acid to run, while the fermentation of sucrose releases 227.5 kJ/mol of lactic acid produced. From a thermodynamic point of view, considering only the enthalpy of formation, the fermentative process would be more efficient than the hydrothermal process. This efficiency may be lower because these values do not consider the energy required for heating, agitation and other energy requirements.

Reaction conditions are milder for the fermentative process, with temperatures ranging from ambient to 40 °C and atmospheric pressure. The processing time, however, is very long, with processing times over 8 h (Göksungur *et al.*, 2005; Hugenholtz and Kleerebezem, 1999; Schepers *et al.*, 2006; Zhang and Vadlani, 2013). The hydrothermal process requires higher temperatures and pressure, but has a very short reaction time. This time difference leads to a higher productivity of the hydrothermal process. The fermentative process requires the separation of the lactic acid from a more complex mixture that contains microorganisms, fermentation broth, residual sugars, lactic acid and other organic acids in lower concentration (Guilherme *et al.*, 2011; Silveira *et al.*, 2010). This complexity may lead to higher costs in the separation process, while the hydrothermal process requires a less complex separation system.

## CONCLUSIONS

The results showed that the use of high concentrations of glycerol in the hydrothermal process increased the productivity and concentration of lactic acid in the reaction medium. The higher productivity however, was obtained at the expense of a lower yield of conversion of glycerol into lactic acid. At the optimal operating conditions, the hydrothermal process was able to produce lactic acid with higher productivities and concentrations of lactic acid than the fermentative process (currently the main industrial route for lactic acid production).

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