

Flash Pyrolysis of Oleic Acid as a Model Compound Adsorbed on Supported Nickel Catalysts for Biofuel Production

Roger Fréty,^a Marilia R. Santos,^a Renan F. Sales,^a Antonio O. S. Silva,^b Celmy B. M. Barbosa^a and Jose G. A. Pacheco^{*,a}

^aDepartmento de Engenharia Química, Centro de Tecnologia e Geociências, Universidade Federal de Pernambuco, 50740-521 Recife-PE, Brazil

^bDepartmento de Engenharia Química, Centro de Tecnologia, Universidade Federal de Alagoas, 57072-970 Maceió-AL, Brazil

A pirólise rápida do ácido oleico foi estudada sobre catalisadores com 10% Ni suportados em sílica e alumina. Os catalisadores foram impregnados com 10% m/m de ácido oleico. Os precursores secos e os catalisadores contendo ácido oleico foram caracterizados por análise termogravimétrica. Os catalisadores calcinados foram analisados por difração de raios X (XRD) e redução à temperatura programada (TPR). As amostras com ácido oleico adsorvido foram submetidos à pirólise rápida a 650 °C. A pirólise de ácido oleico puro levou a 10% de conversão, enquanto a pirólise catalítica resultou em praticamente completa conversão. O catalisador NiO/alumina produziu mais hidrocarbonetos do que o NiO/sílica. Os principais produtos obtidos com NiO/sílica foram 1-alcenos, enquanto que os principais produtos obtidos com NiO/alumina foram isômeros de alcenos e aromáticos, e pequenas quantidades de compostos oxigenados, principalmente álcoois. A pirólise rápida de ácido oleico adsorvido em catalisadoras representa um método útil para distinguir as propriedades dos catalisadores e suas diferentes atividades.

Flash pyrolysis of oleic acid was studied over 10 wt.% nickel catalysts supported on silica and alumina. The catalysts were impregnated with 10 wt.% oleic acid. The dried precursors and the catalysts containing oleic acid were characterized by thermogravimetric analysis. The calcined catalysts were analyzed by X-ray diffraction (XRD) and temperature programmed reduction (TPR). Samples containing adsorbed oleic acid were submitted to flash pyrolysis up to 650 °C. Whereas pyrolysis of oleic acid without catalyst converted only about 10%, the pyrolysis of oleic acid adsorbed on catalysts allowed practically a complete conversion. NiO/alumina yielded a higher amount of liquid hydrocarbons than NiO/silica. The main products obtained with NiO/silica were 1-alkenes, whereas the main products obtained with NiO/alumina were alkene isomers and aromatics. Small amounts of oxygenated compounds were also observed, principally alcohols. The flash pyrolysis of oleic acid adsorbed on different catalyst surfaces appears as a useful way to distinguish activity trends of different catalyst samples.

Keywords: flash pyrolysis, biofuel, oleic acid, nickel catalysts

Introduction

Upgrading of vegetable oils and related compounds to obtain liquid fuels has been extensively studied since the end of the 70's. Two important chemical routes have been used: transesterification and thermochemical processes, these latter either through cracking or hydrocracking.¹⁻⁶

Transesterification is the process usually employed at the industrial level. In this case, vegetable oils react with a short chain alcohol to form esters of fatty acids. These esters are usually named biodiesel. Industrially, methyl esters of fatty acids can be added to petroleum diesel up to 7-8 wt.%. These mixtures, unlike pure petroleum diesel, show a slightly lower energetic power due to their oxygen content and they have limited chemical stability.⁷ Therefore, stabilizers must be added to biodiesel to render it useful.^{8,9} The thermochemical routes can lead to highly deoxygenated compounds fully miscible with liquid fuels of fossil origin.⁵ Companies, such as UOP LLC, Neste Oil, Petrobras and Eni S. p. A., have studied hydrocracking of

^{*}e-mail: jose.pacheco@ufpe.br, geraldo.ufpe@gmail.com

triglycerides with catalysts similar to the ones used in the hydrotreatment processes. For example, Eni S. p. A. and UOP LLC are using the EcofiningTM technology to obtain green diesel, a qualitative biofuel.¹⁰ When carried out in the presence of hydrotreating-type catalysts, at hydrogen pressures higher than 3 MPa and at temperatures between 300-400 °C, hydrocracking of triglycerides leads to important amounts of saturated linear hydrocarbons, with a high selectivity towards C16-C18 molecules.^{5,11} During hydrocracking two main routes have been observed: decarboxylation and decarbonylation (DCO). In both of these reactions the triglycerides are initially transformed into fatty acids that can lose CO_2 and $CO + H_2O_2$, producing hydrocarbons which have a carbon chain with one less C atom than the fatty acid from the initial feed.⁵ A third reaction is also observed in the presence of hydrogen and is considered as hydrodeoxygenation (HDO). In this case, oxygen is eliminated from the intermediate fatty acid as H₂O and the main hydrocarbon molecules formed have the same carbon number as the starting fatty acid chain.5 Because the HDO reaction consumes important amounts of hydrogen, studies aiming at favoring DCO over HDO are important. Kubicka and Kaluza¹² showed that hydrotreating-type catalysts containing only Mo species favor HDO during rapeseed oil hydrocracking, whereas the addition of Ni favors DCO. Kubicka et al.13 also showed that Ni-Mo catalysts with the same composition and the same method of preparation have HDO activity varying with the nature of the support. Therefore, modification of the composition of catalysts appears as an effective way to direct hydrocracking of triglycerides towards DCO.

In order to limit hydrogen consumption, cracking of triglycerides and/or model compounds in the absence of added hydrogen has been considered. Cracking without a catalyst leads to a large family of deoxygenated liquid organic compounds, such as alkenes and alkanes, together with oxygenated compounds, such as carboxylic acids, ketones, aldehydes and alcohols.¹⁴⁻¹⁷ When using catalysts, the degree of deoxygenation is generally enhanced.¹⁸ In such cases, the C number in the products is not always lower than the C number of the original feed.¹⁹⁻²¹ When the catalysts have strong acid sites, the amount of liquid alkenes and alkanes is decreased whereas important amounts of aromatic compounds are formed.²²

Numerous studies have considered the use of model compounds to help understand some mechanistic aspects of the decomposition of triglyceride molecules due to their high complexity. Together with the cracking of saturated fatty acids, like stearic and palmitic acids formed during the hydrocracking of triglycerides, the use of oleic acid as a model molecule has been used to simulate what can

occur in the absence of added hydrogen.²¹⁻²⁹ A recent study on the pyrolysis of oleic acid in an autogeneous atmosphere, between 350 and 450 °C, confirmed that both decarboxylation and decarbonylation took place in the reactor, but also revealed internal cracking at the allylic C position, leading to a predominance of C6-C10 hydrocarbons in the liquid products and the formation of C9 and C10 fatty acids.³⁰ The amount of fatty acids decreased when the temperature of pyrolysis was increased, whereas the amount of mono- and poly-aromatic compounds increased. A recent study from our group described the flash pyrolysis of micro amounts of fatty compounds adsorbed on different solid catalysts, NaZSM-5, HZSM-5, γ-alumina, SAPO-5 and NiMo/SAPO-5, as a rapid way to screen some catalyst properties and confirm the presence of even minute amounts of products, especially primary reaction intermediates.³¹

The present work studies the flash pyrolysis of oleic acid, as it is the main fatty acid in most triglycerides taken from vegetable oils. Supported nickel catalysts were used to increase the deoxygenation process. We pre-adsorbed a very small amount of oleic acid on the surface of the catalysts in order to limit the influence of pyrolysis without catalyst. Thus, we could study the role of the catalyst in the initial steps of the decomposition of oleic acid.

Experimental

Preparation of the catalysts

Supported nickel catalysts with 10 wt.% Ni (as NiO) were prepared by impregnation with an excess of aqueous solution of nickel(II) nitrate hexahydrate (Merck PA). The supports used were a transition alumina (Pural Sasol), and a commercial silica (Kali Chemie AF125), both in powder form. The solids obtained after evaporation in a rotating device were dried at 110 °C in static air, manually ground for homogenization and calcined under air at 650 °C (heating rate of 10 °C min⁻¹) to generate the calcined catalysts precursors. Supports impregnated with pure water were treated in the same way as the supported catalysts in order to have a true reference carrier when necessary.

Addition of oleic acid onto the catalysts

NiO/silica and NiO/alumina after a new drying at $150 \,^{\circ}$ C were mixed with small amounts of pure oleic acid (OA) (Sigma Aldrich > 93%), in a mass proportion of 1 g of catalyst for 0.1 g of OA, under permanent manual agitation to allow complete spreading of the OA. At the end of this "pseudo" impregnation, the catalysts maintained their powder form. They are referred to as OA/NiO/support in

the following sections. The use of a high catalyst:reactant ratio was to provide high availability of catalytic sites and minimize the influence of thermal pyrolysis.

Characterization of the catalysts

Pure nickel nitrate and nickel nitrate deposited on both supports at the end of the drying treatment, as well as OA/NiO/silica and OA/NiO/alumina, were characterized by thermogravimetric/differential thermal analysis (TG/DTA) using a Perkin Elmer STA 6000 instrument. The experiments were conducted under a synthetic airflow rate of 20 mL min⁻¹ between 30 and 600 °C at a heating rate of 10 °C min⁻¹. The reduction of supported NiO was done using a homemade temperature programmed reduction (TPR) equipment, at a heating rate of 10 °C min⁻¹ up to 800 °C, using a mixture of H₂/argon (1.5 vol.% of hydrogen) with a gas flow rate of 70 mL min⁻¹. The supports, the calcined NiO supported samples and the reduced catalysts at the end of TPR were characterized by X-ray diffraction (XRD) (Shimadzu diffractometer, model 6000) using the CuK α radiation, between 10 and 80° at a scanning rate of 2° min⁻¹. The accelerating voltage and the current employed were 40 kV and 30 mA, respectively. The acidity of the catalysts was determined by using pyridine as probe molecule in the same TG Perkin Elmer equipment. An amount of 3 mg of catalyst was pre-treated from 35 to 110 °C for 30 min to remove humidity and then heated to 550 °C at 20 °C min⁻¹ to remove chemisorbed water. After cooling the sample an amount of 1 µL of pyridine per mg of catalyst was carefully added to the catalyst at 120 °C. The desorption of pyridine excess was carried out at the same temperature until reaching equilibrium, after about 60 min. The chemisorbed pyridine was desorbed by heating up to 550 °C at 10 °C min⁻¹ and the loss of mass was recorded with temperature. Specific surface area of the catalysts was determined by the Brunauer-Emmett-Teller (BET) method in a Quantachrome NOVA-2000 equipment at 77 K (-196 °C) with nitrogen adsorption. Samples were pre-treated at 250 °C for 2 h under vacuum before measurement.

Flash pyrolysis experiments

The flash pyrolysis of pure OA and OA adsorbed on both NiO/supported samples were performed in a Pyroprobe CDS-5200 micropyrolysis set up, linked to a gas chromatography/mass spectrometry (GC/MS) analysis system (Shimadzu GC-MS QP 2010 Plus). The powdered sample of the OA/catalyst was placed in a 2 mm × 25 mm quartz tube between quartz wool plugs, in an amount of around 1.0 mg of catalyst with 0.1 mg of impregnated oleic acid. The quartz tube was placed inside a resistive platinum coil heater. The flash pyrolysis was conducted at 650 °C for 0.25 min, at a heating rate estimated as 1000 °C min⁻¹ with a helium flow rate through the sample of 150 mL min⁻¹. After pyrolysis, the vapors and gases flowed to the GC injector through a transfer line heated at 170 °C, as shown in Figure 1. The chromatographic analysis was performed in a DB-5MS analytical column ($30 \text{ m} \times 0.25 \text{ mm} \times 0.25 \text{ }\mu\text{m}$), with a helium flow rate through the column of 1 mL min⁻¹. The column program was 5 min at 45 °C, heating to 280 °C at a heating rate of 4 °C min⁻¹, with a 10 min stay at 280 °C. The ion source was maintained at 280 °C and the interface at 290 °C. The m/z data were measured between 40 and 400. The chromatographic peaks of the pyrolysis products were identified using the National Institute of Standards and Technology (NIST) library standards as well as comparing with data from the literature. The probability of products identification was better than 90% for the great majority of the peaks. The standard deviations of the main peaks in some replicated experiments were smaller than 25%.

Results and Discussion

Characterization of the catalysts

Figure 2 presents TG and derivative thermogravimetry (DTG) curves obtained during the decomposition of nickel nitrate hexahydrate either pure or impregnated on both alumina and silica. The decomposition of pure nickel nitrate shows four main mass losses, with maxima at around 100, 180, 240 and 320 °C. The three low temperature mass losses



Figure 1. Pyroprobe reactor system (not to scale): sample in a 2 mm \times 25 mm quartz tube, platinum coil heater; transfer line to the GC injector; GC chromatograph; MS detector.

are attributed to water loss, whereas the high temperature event is due to NO, release.^{32,33} Above 650 °C, no further mass loss was observed suggesting a complete decomposition of pure nickel nitrate to nickel oxide. In the presence of both supports, a first mass loss ending between 150 and 170 °C is attributed to water release from the support. Further mass losses vary with the nature of the support, a clear mass loss process appearing only with nickel nitrate deposited onto silica, with a maximum rate at around 270 °C. The other steps are not well resolved. Table 1 shows the mass loss percentage from the decomposition of pure or supported nickel nitrate on silica and alumina, obtained from the TG curves. Figure 2 and Table 1 show that the decomposition temperature of the nickel nitrate for the release of NOx follows the order: NiO/alumina > NiO/silica. This suggests that the interaction of the nickel with alumina is higher than with silica.

The DTA curves presented in Figure 3 show some similarities to the DTG curves, all thermal processes being endothermic. For pure nickel nitrate, there are five



Figure 2. TG (a) and DTG (b) curves under air atmosphere for nickel nitrate, either pure or impregnated on both silica and alumina, up to 600 $^{\circ}$ C (10 $^{\circ}$ C min⁻¹).



Figure 3. DTA curves under air atmosphere for nickel nitrate, either pure or impregnated on both silica and alumina, up to $600 \text{ }^{\circ}\text{C} (10 \text{ }^{\circ}\text{C min}^{-1})$.

main peaks, the first one with a maximum at 50 °C, due to both a fusion process of the hydrated salt and the loss of a first molecule of water. The second, third and fourth events at around 100, 200 and 250 °C are essentially due to water release, whereas the fifth one, with a maximum at around 320 °C is due to NO_x elimination. For the supported materials, the low temperature endotherm is due to water elimination from the supports, the process ending at 180 °C. The endothermic peaks observed at around 270 °C for both nickel/silica and nickel/alumina precursors are attributed to NO_x elimination. In this latter case a stronger interaction of the nickel precursor with alumina decreases the decomposition rate of the precursor. TG curves in Figure 2a show that the decomposition of nickel nitrate on silica is faster than on alumina. In both Figures 2 and 4, no further mass loss and/or clear thermal event occurs above 500 °C, suggesting that the precursor salt of nickel is fully decomposed at this temperature. The difference in decomposition behavior between both supported materials suggest that the interaction of the impregnated nickel salt is different on both supports, a situation that may lead to different interactions with the support of the NiO particles formed at the end of heat treatment, in agreement with data from the literature.³⁴

Table 2 gives some properties of the supported catalysts either in oxidized or reduced form such as temperature reduction interval, crystallite mean size, specific surface area and acidity. This table shows that the reduction of NiO/silica is completed at 460 °C, whereas the reduction of NiO/alumina is completed at 750 °C. The rather low reducibility of the present supported NiO is essentially due to the experimental conditions used, where the partial pressure of hydrogen is low. As the reduction rate of

Material	1 st Temperature water release / °C	1 st Mass loss / %	2 nd Temperature water release / °C	2 nd Mass loss / %	3 rd Temperature NOx release / °C	3rd Mass loss / %	
Ni(NO ₃) ₂ .H ₂ O	30-150	29	150-260	19	260-390	43	
Ni nitrate/silica	30-150	65	150-220	9	220-320	18	
Ni nitrate/alumina	30-120	39	120-170	4	170-310	30	

Table 1. Mass loss percentage from the decomposition of pure or supported nickel nitrate on silica and alumina, from the TG curves



Figure 4. X-ray diffractograms of silica, NiO/silica, alumina, NiO/alumina after calcination at 650 °C and reduced Ni/silica and Ni/alumina after TPR at 800 °C.

unsupported nickel oxide presents a positive reaction order regarding the hydrogen pressure, the low pressure used in the present TPR experiments does not favor the metal reduction, but it may allow possible NiO-support interactions during the heating ramp, increasing the temperature of the reduction process. Such situation may affect the final state of the reduced nickel.³⁵ The reduction temperature of nickel oxide on alumina is higher than on silica suggesting that the interaction of NiO with alumina is higher than with silica. A limited formation of nickel aluminate, at the interface between alumina and supported NiO particles, can also be advocated to explain the lower reducibility of alumina supported nickel oxide. This situation will be further discussed during the analysis of XRD data (Figure 4). Table 2 also shows that the specific surface area of NiO/silica is twice as much the area of NiO/alumina. The acidity of NiO/alumina (0.15 mmol of pyridine g^{-1}) is almost three time higher than the acidity of NiO/silica.

Figure 4 presents the XRD diffractograms for silica, NiO/silica, reduced Ni/silica after TPR, alumina, NiO/alumina and reduced Ni/alumina. The XRD results of the silica supported catalyst present a wide peak at $2\theta = 22^{\circ}$, due to the *quasi* amorphous structure of the silica and diffraction lines at $2\theta = 37$, 43, 63° typical of NiO.³⁶ Diffraction lines attributed to metallic nickel Ni⁰ ($2\theta = 45$, 52 and 76°) are observed after TPR, the amorphous line of silica support being unaltered. Therefore, on silica, supported NiO is obtained at the end of the calcination at 650 °C of the supported nickel nitrate, and metallic nickel at the end of TPR.

In Figure 4, the XRD diagram of alumina is very typical of transition alumina. The lines at $2\theta = 19, 32$, 37, 39, 45, 60 and 67° are close to those described in the case of γ -alumina.³⁷ In this case, peaks due to alumina and NiO are partially merged. Only the diffraction lines of NiO at 43 and 63° are clearly observed. This observation confirms that with alumina, NiO is also obtained at the end of the calcination at 650 °C. However, Figure 3 shows that the presence of nickel aluminate NiAl₂O₄ cannot be ruled out since its XRD lines overlap with the lines characteristic of transition alumina.³⁸ After TPR, Ni⁰ diffraction lines are clearly present at $2\theta = 52$ and 76° . Therefore, although the reduction process of the catalyst supported on alumina requires higher temperature under TPR conditions than the reduction of the catalyst supported on silica, the reduction mainly transforms NiO to metallic nickel in both cases. We were able to estimate a crystallite size of

Table 2. Reduction temperature of NiO to metalic nickel from TPR, NiO or Ni crystallite particle size and specific surface area and acidity of NiO/silica and NiO/alumina

Catalyst	Reduction temperature / °C	NiO or Ni crystallite size /nm	Specific surface area / (m ² g ⁻¹)	Acidity / (mmol pyridine g ⁻¹)		
NiO/silica	-	22.1	308	0.06		
NiO/alumina	-	12.5	152	0.15		
Ni ⁰ /silica	340-460	15.0	-	_		
Ni ⁰ /alumina	440-750	9.0	_	_		

15 nm for Ni⁰/silica and smaller than 9 nm in the case of Ni⁰/alumina using the Scherrer equation with the diffraction line at 52 and 76° (Table 2).³⁹ Therefore, after reduction, the Ni crystallite size is different on silica and alumina, probably as a consequence of the differences of NiO interaction with both supports. These differences of interaction probably started during impregnation/drying and/or decomposition processes of the nickel precursor as suggested by the different decomposition profiles observed in both DTG (Figure 2) and DTA (Figure 3). Table 2 also shows that the particle size of NiO on silica is bigger than the size of NiO on alumina.

DTG of oleic acid, either pure or adsorbed on NiO/support catalysts

Figure 5 presents the TG and DTG curves obtained under nitrogen atmosphere for OA/NiO/silica, OA/NiO/alumina and pure OA as reference. For pure OA, a single mass loss



Figure 5. TG (a) and DTG (b) curves under nitrogen atmosphere for pure OA and OA adsorbed on both NiO/silica and NiO/alumina, up to 600 $^{\circ}$ C (10 $^{\circ}$ C min⁻¹).

is observed with the maximum rate at around 260 °C. In the case of OA adsorbed on both catalysts, after a mass loss before 150-200 °C attributed essentially to water desorption from the catalyst surface, the main mass loss occurs at higher temperatures by comparison with pure OA mass loss. Thus, the adsorption of OA onto the catalysts increases the temperature of the mass loss due to OA release and/or decomposition. Furthermore, the differences in mass loss profiles for pure OA and OA adsorbed on both NiO/alumina and NiO/silica catalysts, as well as the differences in the temperature of maximum mass loss rate, indicate that the strength of OA adsorption varies with the nature of the catalyst. Consequently, it can be supposed also that the pyrolysis of OA, either unsupported or supported on both catalysts will generate different families of products, both catalysts retaining more strongly some pyrolysis products when compared with pyrolysis without catalyst. One further point must be added: above 600 °C, no clear mass loss event is observed, justifying in part, together with literature data,¹⁷ the choice of 650 °C as the final flash pyrolysis temperature used in the next section.

Flash pyrolysis of oleic acid, either pure or adsorbed on NiO/support catalysts

Figure 6 shows the peaks of products (pyrogram) obtained during the flash pyrolysis at 650 °C of pure OA and OA adsorbed on both NiO/silica and NiO/ alumina. Table 3 summarizes the main classes of products identified. During the pyrolysis of pure OA, the percentage of the products formed up to the retention time of 41.1 min represents less than 10% of the whole area of the pyrogram. The main peaks on the right side of the pyrogram, with retention times equal and higher than 41.1 min are due to C14 and C16 fatty acids and to untransformed C18 oleic acid (retention time of 52 min). That part of the pyrogram represents more than 90% of the area of the whole pyrogram. Therefore, during the flash pyrolysis of pure OA at 650 °C, fatty acids with shorter C chain are obtained before DCO can occur. At retention times lower than 41.1 min, many other oxygenated products are found: among them, dodecanoic (0.25%), undecylenic (0.16%), decanoic (0.41%), octanoic (0.31%), 7-octenoic (0.07%), heptanoic (0.10%) and acetic (0.09%) acids are identified. Aldehydes, alcohols and ethers are also identified. Finally, the amount of deoxygenated compounds, mainly monounsaturated alkenes, does not represent more than 3.8% of the whole pyrogram. Hence, the flash pyrolysis of pure OA in the present experimental conditions is limited and does not favor deoxygenation.



Figure 6. Total ion chromatograms showing the products from flash pyrolysis for pure oleic acid (OA) (a) and of OA adsorbed on both NiO/silica (b) and NiO/alumina (c).

 Table 3. General distribution of compounds analyzed at the end of flash pyrolysis of pure OA, and OA adsorbed on both NiO/silica and NiO/ alumina

System	NI area / %	OC area / %	HC area / %
OA	25.30	71.78	3.82
OA/NiO/silica	11.46	8.47	80.07
OA/NiO/alumina	13.50	5.92	78.57

NI: Non-identified compounds; OC: oxygenated compounds; HC: deoxygenated compounds (hydrocarbons).

The two pyrograms obtained when OA is adsorbed on both NiO/silica and NiO/alumina hardly show the presence of residual unconverted OA: the contact between the catalyst surface and the adsorbed OA allows a complete transformation of oleic acid. Contrary to pyrolysis without catalyst, the pyrolysis in the presence of catalysts reveals the formation of a very important amount of light products. Among these products it is possible to observe peaks due to homologous compounds like 1-alkenes (peaks 1, 3, 4, 5, 6), as shown in Figure 7, where the names of organic compounds are attributed to some peaks between the retention times of 5 and 25 min.

Table 4 gives the semi-quantitative distribution of the deoxygenated compounds (area percentage of saturated, monounsaturated, polyunsaturated and aromatic compounds). Whereas Table 3 indicated that the amount of deoxygenated compounds (hydrocarbons) is practically similar for both OA/NiO/alumina and OA/NiO/silica, Table 4 shows important differences between the distribution of the hydrocarbon families obtained after pyrolysis at 650 °C of OA adsorbed onto both catalysts: in the case of NiO/alumina, the pyrolysis of OA leads to an important amount of aromatic products, a family



Figure 7. Total ion chromatograms between retention times 5-25 min of the products from flash pyrolysis for pure oleic acid (OA) (a) and of OA adsorbed on both NiO/silica (b) and NiO/alumina (c). The main compounds in pyrogram (b) are: (1) octene, (2) *n*-octane, (3) 1-nonene, (4) 1-decene, (5) 1-undecene, (6) (*E*)-2-undecene, (7) 1,4-undecadiene, (8) 1-dodecene, (9) 6-dodecyne.

 Table 4. Area percentage of the deoxygenated products formed during the flash pyrolysis of AO either pure or adsorbed on both NiO/silica and NiO/alumina

System	SAT area / %	MO area / %	PO area / %	A area / %		
OA	0.33	2.59	0.92	0		
OA/NiO/silica	10.82	51.19	14.72	3.34		
OA/NiO/alumina	6.60	42.30	8.12	21.55		

SAT: Saturated; MO: monoolefins; PO: polyunsaturated hydrocarbons; A: aromatics.

of compounds produced in a much lower amount with OA/NiO/silica. On the other hand, OA/NiO/silica produces more alkanes, alkenes and polyunsaturated hydrocarbons, such as dienes, trienes and alkynes than OA/NiO/alumina.

Table 5 identifies the main aromatic products formed during pyrolysis with both catalysts. In the case of pyrolysis of OA without catalyst, no aromatic compound was detected analyzing peaks with a percentage area equal to or higher than 0.06%. For OA/NiO/silica, together with benzene, linear alkylbenzenes with lateral chain containing 1, 2, 3, 4 and 6 C were found, as well as one dialkyl benzene. For OA/NiO/alumina, more than 50 aromatic compounds were detected, among them linear alkylbenzenes, with lateral carbon chain between 1 and 11 C, representing more than 50% of all the aromatic compounds detected. A few number of alkenyl benzenes, an important number of di- and trialkyl benzenes and a rather large number of polyaromatic compounds, such as indane/indene, naphthalenes and fluorene, either unalkylated or with limited alkyl chains, were also identified.

Table 6 summarizes the amounts of monoalkyl benzenes formed with both OA/NiO/silica and OA/NiO/alumina. Monoalkyl benzenes have been observed in preceding studies dealing with cracking/hydrocracking of fatty compounds, but up to the time of our study, a general sequence of alkyl benzenes as observed with OA/NiO/alumina

Table 5. Main aromatic compounds formed during the pyrolysis of oleic acid adsorbed on both NiO/alumina and NiO/silica. The second column is the retention time t_R (min), the third is the name of the aromatic compound, the fourth is the chemical formula, the fifth and sixth are the area percentage from the pyrogram, respectively on NiO/alumina and NiO/silica

entry	t _R / min	Compound	Formula	NiO/alumina	NiO/silica
1	2.897	Benzene	C ₆ H ₆	2.89	1.28
2	4.783	Toluene	C_7H_8	3.41	0.78
3	8.088	Ethylbenzene	C_8H_{10}	1.24	0.34
4	8.470	<i>m-p</i> -Xylene	$C_8 H_{10}$	0.57	_
5	12.097	Propyl-benzene	$C_{9}H_{12}$	0.64	0.31
6	12.436	1-Ethyl-3-methyl-benzene	$C_{9}H_{12}$	0.19	_
7	13.188	1-Ethyl-2-methyl-benzene	C_9H_{12}	0.81	-
8	13.140	(1-Methylethyl)-benzene	C_9H_{12}	-	0.15
9	13.968	1-Propenyl-benzene	C_9H_{10}	0.63	_
10	15.053	1,2,4-Trimethyl-benzene	$C_{9}H_{12}$	0.09	-
11	15.618	Indane	C_9H_{10}	0.25	-
12	16.041	Indene	C_9H_8	0.53	_
13	16.386	1-Methyl-3-propyl-benzene	$C_{10}H_{14}$	0.13	_
14	16.618	Butyl-benzene	$C_{10}H_{14}$	0.55	0.28
15	16.990	1-Methyl-4-propyl-benzene	$C_{10}H_{14}$	0.58	-
16	17.347	(E)-1-Butenyl-benzene	$C_{10}H_{12}$	0.10	_
17	17.436	1-Ethyl-2,3-dimethyl-benzene	$C_{10}H_{14}$	0.08	_
18	17.547	1-Methyl-2-(1-methylethyl)-benzene	$C_{10}H_{14}$	0.09	_
19	17.680	1-Methyl-1,2-propadienyl-benzene	$C_{10}H_{10}$	0.10	-
20	17.819	1-Phenyl-1-butene	$C_{10}H_{12}$	0.17	-
21	19.363	(2-Methyl-1-propenyl)-benzene	$C_{10}H_{12}$	0.17	-
22	19.529	(E)-1-Butenyl-benzene	$C_{10}H_{12}$	0.07	-
23	19.779	2,4-Dimethylstyrene	$C_{10}H_{12}$	0.07	_
24	20.083	2,3-Dihydro-4-methyl-1H-indene	$C_{10}H_{12}$	0.11	_
25	20.197	1,3-Diethyl-5-methyl-benzene	$C_{11}H_{16}$	0.31	_
26	20.439	3-Methyl-1 <i>H</i> -indene	$C_{10}H_{10}$	0.55	_
27	20.754	1-Methyl-1H-indene	$C_{10}H_{10}$	0.40	-
28	21.160	1-Methyl-4-(2-methylpropyl)-benzene	$C_{11}H_{16}$	0.56	-
29	21.941	Azulene	$C_{10}H_{8}$	0.64	_
30	23.036	(1-Methyl-1-butenyl)-benzene	$C_{11}H_{14}$	0.09	-
31	23.346	1-Methyl-2-(1-ethylpropyl)-benzene	$C_{12}H_{18}$	0.10	_
32	23.484	trans-1-Phenyl-1-pentene	$C_{11}H_{14}$	0.07	_
33	24.046	1-Ethyl-4-(2-methylpropyl)-benzene	$C_{12}H_{18}$	0.19	_
34	24.846	Hexyl-benzene	$C_{12}H_{18}$	0.48	0.20
35	25.030	(1,3-Dimethylbutyl)-benzene	$C_{12}H_{18}$	0.62	-
36	25.142	2,3-Dimethyl-1H-indene	$C_{11}H_{12}$	0.20	_
37	26.756	1-Methyl-naphthalene	$C_{11}H_{10}$	0.35	_
38	28.625	Heptyl-benzene	$C_{13}H_{20}$	0.51	_
39	28.738	1-Methyl-2-n-hexylbenzene	$C_{13}H_{20}$	0.36	_
40	29.806	2-Methyl-1,1'-biphenyl	C ₁₃ H ₁₂	0.19	-
41	30.704	2,3-Dimethyl-naphthalene	$C_{12}H_{12}$	0.06	_
42	32.159	Octyl-benzene	$C_{14}H_{22}$	0.41	_
43	32.253	(1-Methylheptyl)-benzene	$C_{14}H_{22}$	0.25	-
44	35.519	Nonyl-benzene	C115H24	0.55	-
45	35.561	(1-Methyl-nonyl)-benzene	C ₁₆ H ₂₆	0.43	-
46	35.921	Fluorene	C ₁₃ H ₁₂	0.36	-
47	41.672	Undecyl-benzene	$C_{17}H_{28}$	0.34	_

has not been reported.^{30,40} In the industrial production of linear alkyl benzenes for detergent applications, the alkylation of olefins is conducted in the presence of a strong acidic medium, either with HF, or more recently with zeolite-type heterogeneous catalysts.^{41,42} The mechanism of this type of catalytic alkylation implies the participation of carbocations and acidic sites. Such a mechanism is rather unexpected under present conditions, although the carboxylic moieties may form acidic OH groups on metallic or support surface sites after adsorption of the acidic function under the form of carboxylate species.^{43,44} However, alumina-supported nickel catalysts have shown very high activity and selectivity in the alkylation of benzene with propene to form cumene.45 Therefore, alkylation with supported nickel catalysts is possible, although the conditions of the present study are different from the conditions used by Jian et al..45 Maybe under the present experimental conditions, the linear alkyl benzenes have essentially been formed through an internal aromatization after or during decarboxylation. Molecules, such as linear alkyl cyclopentenes or linear alkyl cyclohexenes able to lose hydrogen on nickel sites to transform the alkylated cycloolefins to alkylated benzenes, are probably used as intermediate molecules. In fact, small amounts of cyclopentenes with linear alkyl chain containing 3, 4, 5, 7 and 8 C, and cyclohexenes with linear alkyl chain with 4 and 6 C have been identified. However, the exact mechanism of formation of the family of alkylbenzenes during the pyrolysis of OA adsorbed on NiO/alumina is still unkown.

Table 7 shows the amounts of linear 1-alkenes in the 3 experiments. Whereas this amount is very limited for the pyrolysis of OA without catalyst (1.8%), both NiO/ alumina (20.7%) and principally NiO/silica (33.5%) decomposed OA towards 1-olefins with satisfactory

selectivity. Although both catalysts help to decompose the adsorbed OA fully, differences in product distribution is clearly observed. It seems evident that the higher acidity of NiO/alumina compared with NiO/silica (Table 2) must play an important role in the formation of the isomers of linear olefins and in the formation of aromatic compounds, these latter compounds being probably formed also due to the dehydrogenating properties of nickel sites. Hydrogen transfer pathways, advocated for example during the decomposition of saturated fatty acids on activated alumina may probably occur in the present experimental conditions, together with the participation of adsorbed hydrogen on the metallic nickel surface, as hydrocarbons are able to reduce nickel oxide to metallic nickel at temperatures in the 400-500 °C range.^{19,46}

Although the amount of oxygenated compounds is not very high, it is important to indicate that CO₂ and acetates were observed with the NiO/alumina sample, but not with NiO/silica. Such a situation is probably linked to the partial adsorption of oleic acid through carboxylate species on the alumina surface, such species being practically absent when the adsorption occurs on the silica surface.⁴³ Among the other oxygenated compounds, carboxylic acids are observed in greater amount with NiO/silica (1.15%) than with NiO/alumina (0.41%), in agreement with the better deoxygenation properties of this latter catalyst. In the same way, more alcohols are formed when pyrolyzing OA on NiO/silica (5.12%) than on NiO/alumina (2.91%). But a large majority of these alcohol and acid molecules are susceptible to transformation into unsaturated hydrocarbons when the experimental condition is slightly changed, DCO and dehydration being rather frequent reactions. A last point can be mentioned, dealing with the identification of some ketones in the condensable pyrolysate. In this case, the

Table 6. Area percentage of alkylbenzenes formed during the flash pyrolysis of pure OA, and OA adsorbed on both NiO/silica and NiO/alumina as a function of the number of C in the alkyl chain

C number in the alkyl chain	C0	C1	C2	C3	C4	C5	C6	C7	C8	C9	C10	C11	Total area / %
OA	_	_	-	-	-	_	_	_	_	_	_	_	_
OA/NiO/silica	1.3	0.8	0.3	0.3	0.3	_	0.2	-	_	_	_	_	3.2
OA/NiO/alumina	2.9	3.4	1.2	0.6	0.5	0.1	0.5	0.5	0.4	0.6	-	0.3	11.0

Table 7. Distribution of 1-alkenes formed during the flash pyrolysis of oleic acid (OA) and OA adsorbed on both NiO/alumina and NiO/silica

System	C3	C4	C5	C6	C7	C8	C9	C10	C11	C12	C13	C14	C15	C16	C17	Total
OA	0.21	_	0.27	0.34	0.25	0.12	0.10	0.08	0.09	0.08	_	0.10	0.07	0.06	0.06	1.83
OA/NiO/silica	_	_	3.71	7.77	3.78	2.38	2.38	1.75	1.79	1.74	1.24	1.54	1.60	0.61	3.21	33.5
OA/NiO/alumina	_	7.13	_	2.48	1.52	1.57	_	0.99	1.59	1.50	1.07	0.84	0.98	0.46	0.60	20.73

amount of ketones is lower with OA/NiO/silica (0.27) than with OA/NiO/alumina (0.70). This is probably linked to the fact that ketones have been shown to be important intermediate species during the cracking of saturated fatty acids in the presence of activated alumina.^{19,20}

The present results confirm that during the decomposition of oleic acid adsorbed on the catalysts, cooperative processes occur between the support surface and the active phase surface. On the one hand, the products are different from the products obtained during cracking without catalysts and therefore, the thermal decomposition has limited importance; on the other hand, both catalysts also generate not always similar products, indicating that the adsorption properties on both catalysts are different. Therefore, as was advocated in a preceding publication, it is confirmed that the present experimental conditions using flash pyrolysis of adsorbed species can be seen as a "pseudo" catalytic test, helping a description of the potential properties of a catalyst before its use in more classical flow or batch reactors.³¹

Conclusions

The flash pyrolysis of oleic acid adsorbed on supported nickel catalysts generates complete decomposition of the fatty acid whereas the pyrolysis without catalyst allowed a decomposition lower than 10%. The products of pyrolysis with supported nickel catalysts were highly deoxygenated, and hydrocarbon content close to 80% was observed in both cases. The selectivity to hydrocarbons was different for both catalysts: an important amount of 1-alkenes was obtained with oleic acid adsorbed on NiO/silica, whereas NiO/alumina generated more alkene isomers, more polyunsaturated hydrocarbons and more aromatic compounds than NiO/silica. The differences of selectivity can be linked on one hand to hydrogen transfer occurring when alumina is used as support, and on the other hand to different adsorption modes of oleic acid on both catalysts, with the carboxylate species probably being more important with alumina support than with silica support. The flash pyrolysis of adsorbed fatty compounds can be proposed as a quick "pseudo" catalytic test to select catalysts before long term reactions are initiated.

Acknowledgements

Financial support from UFPE, FINEP, PETROBRAS, PRH28/ANP/PETROBRAS and RECAT (Rede Norte Nordeste de Catálise) are acknowledged. This work is centered on nickel catalyst properties, which was one of the elements extensively studied by Roberto F. Souza during his successful career.

References

- Schuchardt, U.; Sercheli, R.; Vargas, R. M.; *J. Braz. Chem. Soc.* 1998, 9, 199.
- Pinto, A. C.; Guariero, L. L. N.; Rezende, M. J. C.; Ribeiro, N. M.; Torres, E. A.; Lopes, W. A.; Pereira, P. A. P.; Andrade, J. B.; *J. Braz. Chem. Soc.* 2005, *16*, 1313.
- 3. Ma, F.; Hanna, M. A.; Bioresour. Technol. 1999, 70, 1.
- Maher, K. D.; Bressler, D. C.; *Bioresour. Technol.* 2007, 98, 2351.
- Kubickova, I.; Kubicka, D.; Waste Biomass Valorization 2010, 1, 293.
- Fréty, R.; Rocha, M. G. C.; Brandao, S. T.; Pontes, L. A. M.; Padilha, J. F.; Borges, L. E. P.; Gonzalez, W. A.; *J. Braz. Chem. Soc.* 2011, *22*, 1206.
- Oliveira, E.; Quirino, R. L.; Suarez, P. A. Z.; Prada, A. G. S.; *Thermochim. Acta* 2006, 450, 87.
- Mittelbach, M.; Gangl, S.; J. Am. Oil Chem. Soc. 2003, 80, 817.
- 9. Dunn, R. O.; Fuel Process. Technol. 2005, 86, 1071.
- http://www.transdolomites.eu/wp-content/uploads/ENI-Ecofining-pdf.pdf accessed in November 2014.
- Gusmao, J.; Brodzki, D.; Djega-Mariadassou, G.; Fréty, R.; Catal. Today 1989, 5, 533.
- 12. Kubicka, D.; Kaluza, L.; Appl. Catal., A 2010, 372, 199.
- Kubicka, D.; Horacek, J.; Setnicka, M.; Bulanek, R.; Zukal, A.; Kubickova, I.; *Appl. Catal.*, *B* 2014, *145*, 101.
- Wisniewski Jr., A.; Wiggers, V. R.; Simionatto, E. L.; Meier, H. F.; Barros, A. A. C.; Madureira, L. A. S.; *Fuel* 2010, *89*, 563.
- Lima, D. G.; Soares, V. C. D.; Ribeiro, E. B.; Carvalho, D. A.; Cardoso, E. C. V.; Rassi, F. C.; Mundim, K. C.; Rubim, J. C.; Suarez, P. A. Z.; *J. Anal. Appl. Pyrolysis* **2004**, *71*, 987.
- Fortes, J. C. P.; Baugh, P. J.; J. Anal. Appl. Pyrolysis 2004, 72, 103.
- 17. Lappi, H.; Alen, R.; J. Anal. Appl. Pyrolysis 2009, 86, 274.
- Prado, C. M. R.; Antoniosi, N. R.; J. Anal. Appl. Pyrolysis 2009, 86, 338.
- Leung, A.; Boocock, D. G. B.; Konar, S. K.; *Energy Fuels* 1995, 9, 913.
- 20. Billaud, F.; Tran Minh, A. K.; Lozano, P.; Pioch, D.; *J. Anal. Appl. Pyrolysis* **2001**, *58*, 605.
- Araujo, L. R. R.; Scofield, C. F.; Pastura, N. M. R.; Gonzalez, W. A.; *Mat. Res.* 2006, *9*, 181.
- Dupain, X.; Costa, D. J.; Schaverien, C. J.; Makkee, M.; Moulijn, J. A.; *Appl. Catal.*, B 2007, 72, 44.
- Maher, K. D.; Kirkwood, K. M.; Gray, M. R.; Bressler, D. C.; *Ind. Eng. Chem. Res.* 2008, 47, 5328.
- Snare, M.; Kubickova, I.; Maki-Arvela, P.; Eranen, K.; Murzin, D. Y.; *Ind. Eng. Chem. Res.* 2006, 45, 5708.
- Maki-Arvela, P.; Kubickova, I.; Snare, M.; Eranen, K.; Murzin, D. Y.; *Energy Fuels* **2007**, *21*, 30.

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- Lestari, S.; Maki-Arvela, P.; Simakova, I.; Beltramini, J.; Lu,
 G. Q. M.; Murzin, D. Y.; *Catal. Lett.* **2009**, *130*, 48.
- Dos Anjos, J. R. S.; Gonzalez, W. A.; Lam, Y. L.; Fréty, R.; Appl. Catal. 1983, 5, 299.
- Reguera, F. M.; Araujo, L. R. R.; Picardo, M. C.; Bello, F. O.; Scofield, C. F.; Pastura, N. M. R.; Gonzalez, W. A.; *Mat. Res.* 2004, 7, 343.
- Madsen, A. T.; Ahmed, E. H.; Christensen, C. H.; Fehrmann, R.; Riisager, A.; *Fuel* **2011**, *90*, 3433.
- Asomaning, J.; Mussone, P.; Bressler, D. C.; J. Anal. Appl. Pyrolysis 2014, 105, 1.
- Sréty, R.; Pacheco, J. G. A.; Santos, M. R.; Padilha, J. F.; Azevedo, A. F.; Brandao, S. T.; Pontes, L. A.; *J. Anal. Appl. Pyrolysis* 2014, *109*, 56.
- Elmasry, M. A. A.; Gaber, A.; Khater, E. M. H.; *J. Therm. Anal.* 1998, 52, 489.
- Brockner, W.; Ehrhardt, C.; Gjikej, M.; *Thermochim. Acta* 2007, 456, 64.
- Jasik, A.; Wojcieszak, R.; Monteverdi, S.; Ziolek, M.; Bettahar, M. M.; *J. Mol. Catal. A: Chem.* 2005, 242, 81.
- Ewans, J. E.; Song, S.; Leon-Sucre, C. E.; *Metall. Mater. Trans. B* 1976, 7, 55.
- Musić, S.; Filipović-Vinceković, N.; Sekovanić, L.; *Braz. J. Chem. Eng.* 2011, 28, 89.

- Souza Santos, P.; Souza Santos, H.; Toledo, S. P.; *Mat. Res.* 2000, *3*, 104.
- Nazemi, M. K.; Sheibani, S.; Rashchi, F.; Gonzalez-DelaCruz, V. M.; Caballero, A.; Adv. Powder Technol. 2012, 23, 833.
- 39. Langford, J.; Wilson, A.; J. Appl. Crystallogr. 1978, 11, 102.
- Rocha Filho, G. N.; Brodzki, D.; Djega-Mariadassou, G.; *Fuel* 1993, 72, 543.
- 41. http://www.uop.com/new-uopcepsa-detal-plus-processtechnology-for-the-production-of-linear-alkylbenzene-lab/ accessed in November 2014.
- 42. de Almeida, J. L. G.; Dufaux, M.; Ben Taarit, Y.; Naccache, C.; *Appl. Catal.*, A **1994**, *114*, 141.
- Hasegawa, M.; Low, M. J. D.; J. Colloid Interface Sci. 1969, 30, 378.
- Wu, N.; Fu, L.; Su, M.; Aslam, M.; Wong, K. C.; Dravid, V. P.; Nano Lett. 2004, 4, 383.
- Jian, P.; Wang, Q.; Zhu, C.; Xu, Y.; *Appl. Catal.*, A **1992**, *91*, 125.
- Tournayan, L.; Charcosset, H.; Fréty, R.; Trambouze, Y.; *Ind. Chim. Belge* 1973, 38, 496.

Submitted: August 15, 2014 Published online: November 14, 2014