Kinetic and Thermodynamic Study in Pozzolanic Chemical Systems as an Alternative for Chapelle Test

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Received: February 20, 2018; Revised: April 06, 2018; Accepted: May 11, 2018

Important properties in cementitious materials, such as concrete, are related to the presence of additives that influence the rigidity and the physical and chemical resistances. For the evaluation of the additive effectiveness, known as pozzolanic activity, a simple procedure, the Chapelle test, is commonly used, and it essentially consists in a reaction between the additive with calcium oxide in aqueous medium. However, such procedure presents limitations in terms of processing time and lack of information regarding the reactions kinetics. In this sense, a simple method based on the kinetic and thermodynamic principles of chemical reactions is proposed, which can be performed using conventional electronic pH sensors. The study provides an alternative methodology with many advantages over the traditional procedure, such as energy and time-savings, more robustness and more confidence. In this paper, three types of silica nanoparticles that can be used as low-cost additives were characterized in relation to their morphology and crystallinity by XRD and SEM, the particles average diameters were obtained and the particles were used for studying the chemical process that takes place during the Chapelle test. Results and the semi-empirical analysis provided strong evidence that the process is an acid-base 1:1 reaction and it was verified that the mean reaction times varied from 64 to 195 min. It is a remarkable result, since the proposed analysis can be performed with simple, fast and low-cost instrumentation and needs only a worksheet software, whereas the Chapelle test takes 16 hours and provides no dynamic information. Besides the limitation that the methodology is not able to quantify and to elucidate the effects of the specific surface area of the particles, which needs a complete BET study, the research provides a significant contribution for the understanding of the pozzolanic process, of great importance in both concrete and ceramic research.

Keywords: Chapelle test, pozzolanic reaction, concrete, silica, quartz.

1. Introduction

The advances in concrete technology rely on the use of mineral admixtures, such as silica fume, in order to produce high-performance products¹. The utilization of those materials enhances the concrete properties, including durability, resistance to chloride corrosion, freezing, thawing, and deicing salting scale^{2,3}.

Additions constituted of siliceous or aluminous materials in finely divided form and generally in the presence of water are usually referred as "*Pozzolana*"^{4,5}. These materials react chemically with calcium hydroxide and produce compounds with cementitious properties^{4,5}.

The effectiveness of these additions is termed pozzolanic activity, being commonly evaluated using the Chapelle test^{4,6}, a simple procedure in which 1 g of the analyzed sample is added to 200 mL of deionized water and 1 g of calcium oxide. The mixture is boiled for 16 h, and then it is filtered and titrated with a I N chloride acid solution, with phenolphthalein indicator, in order to evaluate the amount of calcium oxide that has not taken part in the reaction⁵.

The Chapelle test is relatively simple, but it does not provide information about the dynamic behavior of the chemical process. A first problem that can be pointed out is that a 16 h time is sufficiently long for occurring parallel reactions, such as the acid-base neutralization reaction of the calcium oxide by the carbon dioxide present in the air⁷, giving a false interpretation to the test result.

The test is also not able to quantify common effects in chemical reactions that can change the observed rate⁸, like agitation power, solid-liquid equilibrium effects⁹, reaction limitations by the increase of mass transfer resistance, and so on. Moreover, it does not provide important information about the intrinsic kinetics of the process, which can help to elucidate the mechanism of the reaction⁸.

It is also important to realize that the colorimetric indicators, like phenolphthalein, are not able to provide a specific value of pH, since it has a characteristic range in which its color changes¹⁰. Important errors can be added to the analysis, depending on the color of the analyzed medium and depending on the difficulty of the analyst in differentiating the exact titration equivalence point¹⁰. Such errors are increased if the analyte is in low concentration, and this technique is particularly sensitive to the analyst experience in performing the procedure¹⁰.

In this sense, the objective of the present work is to analyze the kinetics of the pozzolanic reaction process, with three different silica nanoparticles reacting with calcium oxide in aqueous solutions. These materials present relative low-cost, what makes them economically attractive for the use as concrete additives. The studied samples were characterized and chemically tested, providing information about their morphology and about the kinetics of the reactions involved.

In order to help the elucidation of the reaction and to correct the temperature effects on the water ionization chemical equilibrium - the chemical equilibrium constant can reach values one order of magnitude higher than the value for 25 °C (10^{-14}) for temperatures lower than $100 °C^9$ - the principles of the chemical equilibrium thermodynamics and the chemical kinetics are applied to the analysis. A particular mechanism is hypothesized, and it is shown that the test can be performed at lower temperatures and during less time than the ones used for Chapelle test, providing important energy savings and faster analysis. The use of an electronic, simple and non-expensive device - the pH meter - also provides more accuracy and confidence to the results obtained, consisting in a useful and fast methodology for the evaluation of the effectiveness of the pozzolanic addition in concrete.

Due to the wide use of concrete, silica, and other ceramic materials on the urban societies, it is of great importance to understand the intrinsic mechanisms that take place when they interact, making it possible to optimize the processes and to find alternatives friendlier in both the economic and environmental perspectives.

2. Materials and Methods

2.1 Thermodynamic analysis of the aqueous solution

In order to evaluate the dynamics of the pozzolanic reaction, the thermodynamic analysis of the aqueous medium must be analyzed properly and the corrections on pH scale with temperature must be performed. In the absence of such rigorous treatment, the simple reading of the pH meter can lead to results of hydroxide ions concentration one or two orders of magnitude lower than the actual values. For example, a reading of pH equals to 11.2 corresponds to a concentration of OH⁻ ions of 0.0016 mol/L when the temperature is 25 °C, but the value for the temperature of 75 °C, used in this research, is approximately equals to 0.036 mol/L, more than 22 times higher.

For correcting the scales, the authors recommend a construction of a worksheet in a software like Microsoft Excel, with a column for the pH meter readings, a column for the experiment temperature, and a column for each one of the equations listed in the text. The equations constitute an algorithm that should be solved in the indicated order, and it is possible to build a computer routine in Excel VBA for solving the more complex operations, with the any adequate numerical method, such as Newton-Rhapson or even a try-and-error procedure and the equations variables are summarized in Table 1. The integral calculus can be performed using the trapezoidal rule, and all the parameters needed are given in the References. The authors recommend that the parameters are put in fixed cells, and the use of the sheet is not restricted to the pozzolanic analysis - it can be used for the temperature correction of the pH reading in any aqueous medium.

Table 1. Nomenclature a	dopted.
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Variable	Meaning
K	Chemical equilibrium constant
a_i	Chemical activity of species " <i>i</i> "
V _i	Stoichiometric coefficient of species "i"
ΔG	Gibbs energy variation
R	Universal gases constant
Т	Temperature
<i>x</i> _{<i>i</i>}	Molar fraction of species "i"
γ_i	Activity coefficient of species "i"
C_p	Specific heat
ΔH	Enthalpy variation
α	Debye-Hückel proportionality coefficient
Z_i	Ionic charge of species "i"
Ι	Ionic strength of reaction medium
m_i	Molality of species "i"
$\beta_{_{ik}}$	Interaction coefficient between species "i" and "k"
ρ	Solvent density at temperature "T"
$\varepsilon_{_T}$	Solvent dielectric constant at temperature "T"
C_A	Molar concentration of the chemical species "A"
C_{A0}	Initial molar concentration of the chemical species " A "
k	Constant of reaction rate
t	Time of reaction

One of the reactants is the calcium oxide, which is known to elevate the water pH due to the liberation of hydroxide ions, accordingly to Equation 1⁷. The variation in OH⁻ ions is then equals to the variation in CaO dissolved in water, and the CaO instant concentration can be calculated by interpreting the reading of a common electronic pH sensor, which gives the medium pH value when its probe is immersed in the aqueous suspension.

$$CaO_{(s)} + H_2O_{(l)} \rightleftharpoons Ca^{2+}_{(aq)} + 2(OH)^-_{(aq)}$$
(1)

The water chemical equilibrium, expressed in Equation 2⁷, is disturbed by the presence of the hydroxide ions formed, and the equilibrium equation relates the concentration of acid ions, detected by the pH meter, to the concentration of hydroxide ions.

$$H_2 O_{(l)} \leftrightharpoons H^+_{(aq)} + OH^-_{(aq)} \tag{2}$$

The chemical equilibrium is described by the equilibrium constant, K, which correlates the chemical activities of the species in the medium, according to Equation 3^9 .

$$\mathbf{K} = \frac{a_1 a_2}{a_3} = \prod_i a_i^{v_i} \tag{3}$$

In Equation 3, the indexes 1, 2 and 3 represent ion $H^{(+)}$, ion $OH^{(-)}$, and molecule H_2O , respectively. The equilibrium constant is related to the reaction Gibbs energy by Equation 4, and the activity of each specie is related to its molar fraction in solution by Equation 5⁹.

$$\Delta G(T) = -RT \ln K \tag{4}$$

$$a_i = x_i \boldsymbol{\gamma}_i \tag{5}$$

In a defined temperature T, it can be demonstrated from the classic van't Hoff equation that the variation in reaction enthalpy is given by Equation 6⁹. In this equation, ΔC_p is the sum of each reactant and product specific heat multiplied by the respective stoichiometric coefficient, and T_0 is a reference and arbitrary temperature.

$$\int_{T_0}^T \Delta C_p(T) = \Delta H(T) \tag{6}$$

The overall variation in reaction Gibbs energy, in a defined temperature, can be predicted from the variations in reaction enthalpy and in the reactants specific heat by Equation 7. This equation is derived from Equation 6, combined to the Kirchhoff and Gibbs equations⁹, where ΔG^{0} and ΔH^{0} are the reaction Gibbs energy variation and enthalpy variation calculated in the reference temperature T_{0} , respectively.

$$\frac{\Delta G(T)}{RT} = \frac{\Delta G^0 - \Delta H^0}{RT_0} + \frac{\Delta H^0}{RT} - \frac{1}{R} \int_{T_0}^T \frac{\Delta H(T)}{T^2} dT \quad (7)$$

The values of $\Delta H/T$ are well known for the ionization equilibrium of water and are available for a wide range of temperatures¹¹, allowing the calculation of the reaction ΔG with Equation 7. Then, the equilibrium constant can be calculated by applying this result to Equation 4.

As the water is always in large excess, with molar fractions above 0.9, its activity can be predicted by the Lewis-Randall rule¹², and it is equal to the water molar fraction:

$$a_3 = x_3 \tag{8}$$

The activity coefficient of ionic species can be evaluated using the Debye-Hückel model for excess Gibbs energy¹³, which is expressed by Equation 9.

$$\ln \gamma_i = -\frac{\alpha(z_i)^2 \sqrt{I}}{1 + \sqrt{I}} + 2 \sum_{k \neq 3} \beta_{ik} m_k \tag{9}$$

The ionic strength, *I*, is defined by Equation 10. In the water system, the ionic charges are $z_1 = +1$ and $z_2 = -1$. Edwards *et al.*¹³ recommend the use of the values $\beta_{12} = \beta_{21} = 0.25$ kg/mol for the interaction between ions hydrogen and hydroxide.

$$I \equiv \frac{1}{2} \sum_{j=1}^{3} (z_j)^2 m_j \tag{10}$$

In order to evaluate the Debye-Hückel coefficient α , semi-empirical correlations can be applied, such as Equation 11¹⁴. Water density and water dielectric constant are also known for a wide range of temperatures^{15,16}.

$$\alpha = \frac{(1.824829238)\rho^{\frac{1}{2}}}{(\varepsilon_{T})^{\frac{3}{2}}} \cdot 10^{6}$$
(11)

After calculating the chemical activities in the reaction temperature, the species concentration can be evaluated by the application of the activity values in Equation 12, which is derived from Equations 3, 5 and 8.

$$K = \frac{a_{H^+} a_{OH^-}}{a_{H_2O}} = \frac{(x_1 \gamma_1) \cdot (x_2 \gamma_2)}{x_3}$$
(12)

It is important to note that, defining *pH* and *pOH* according to Equations 13 and 14^{10} , Equation 12 is simplified to the well-known Equation 15^{10} when the reaction proceeds under 25 °C.

$$pH = -\log(C_{H^+}) \tag{13}$$

$$pOH = -\log[C_{(OH)^{-}}] \tag{14}$$

$$pH + pOH = 14 \tag{15}$$

2.2 Reaction experiments

In order to evaluate the kinetic behavior of a chemical reaction, it is necessary to analyze and to monitor a physical or chemical parameter which is related to the concentration of the species that are reacting⁸. Examples of such properties comprise the medium refractive index⁸, pH⁸, or viscosity¹⁷.

In this research, reaction experiments were conducted in a bench-scale batch reactor made of glass, with magnetic stirring and external temperature control, and the mixture volume was fixed in 250 mL. The reactions were analyzed with a pH meter Gehaka PG 2000 able to measure pH and the sample temperature, equipped with electrode SC26 Sensoglass, adapted for handling temperatures up to 90 °C (Gehaka, Brazil). The reactions were monitored until no more variation in pH could be observed. The medium was kept at constant temperature, but each experiment was carried out in a different condition, with temperatures varying from 55 to 80 °C.

Three different sources of silica were used: amorphous silica nanoparticles ("*soot*"), microcrystalline quartz, and amorphous commercial "active silica" (Tecnosil, Brazil). These particles were characterized by scanning electron microscopy (SEM) and by X-Ray diffraction (XRD).

The pH values measured by the equipment were converted to hydrogen concentration by applying Equation 13, and the thermodynamic Equations 3 to 12 were applied for the conversion of these data in hydroxide ions concentration. The instant hydroxide concentration is related to the instant calcium oxide concentration by Equation 1, since CaO is the main responsible for the medium alkalinity.

2.3 Nanoparticles preparation

Soot particles were synthesized by the Vapor Axial Deposition (VAD) method, which has been widely studied for the production of optical fiber preforms¹⁸. The silica particles produced by this methodology are completely amorphous and present spherical morphology¹⁸. The particles morphologies can be precisely controlled by adjusting the gases flow rates, such as H₂, O₂, N₂, and SiCl₄ flow rates, and by controlling the burner-target distance *D*, the burner-target inclination angle θ , and the target vertical translation speed v^{18,19}, as shown in Figure 1.



Figure 1. Scheme of the VAD chamber used for the synthesis of soot nanoparticles.

A high-temperature O_2 - H_2 flame promotes the hydrolysis and oxidation of SiCl₄, according to reaction 16. The nanoparticles are axially deposited on the surface of a silica rod target in constant rotation and controlled vertical translation movements¹⁹.

$$SiCl_4 + 2H_2 + O_2 \rightarrow SiO_2 + 4HCl$$
 (16)

After the deposition, a "green body" is formed over the silica rod, as shown in Figure 2. This green body is mechanically separated from the rod and crushed in a silica mortar in order to separate the agglomerated nanoparticles, forming the silica powder (soot).



Figure 2. Green body formed by agglomerated silica nanoparticles synthesized by VAD.

The crystalline quartz microparticles were produced *in-house* using ball milling in silica medium, and quartz lumps were used as balls, in order to minimize the material contamination²⁰. The mill is loaded with the quartz sand and deionized water and is subjected to constant rotation (fill factor K=0.42)²¹. The quartz balls comminute the sand and progressively reduce the crystal dimensions. The milling time was fixed in 165 h, and the rotation speed was set to 100 rpm²².

After the milling process, the mixture of milled quartz and water was transferred to a 2 L graduated cylinder and completed with deionized water. After 48 h, the large particles were sedimented, whereas submicron particles remained floating in the translucid phase, as shown in Figure 3. Then, this clarified portion was separated and the water was evaporated, forming a fine powder, yielding micro and nanostructured crystals.

2.4 Mechanistic hypothesis and integral analysis

Since in standard temperature and pressure conditions (STP) silica can be classified as an acid oxide, weakly ionizable in water, getting a negative charge⁷, and calcium oxide is a basic oxide, as shown in Equation 1, it can be hypothesized that the pozzolanic reaction consists in a Lux-Flood acid-base reaction²³.



Figure 3. Decanting process. After 48h, the translucent phase is drained and the water is evaporated, forming a powder containing submicron particles.

Lux-Flood concept defines acid as a species which is able to receive oxide ions, whereas a base is a species which is able to donate oxide ions²³. Lux-Flood definition is mainly applied to fused oxide and fused salt systems and can be understood as the neutralization of an acid oxide by a basic oxide^{7,23}.

It is important to realize that, in aqueous solutions, the Lewis acid-base definition, by which the base is a species able to donate an electron pair and an acid is a specie able to receive it^{7,23} can be equivalently applied to this system. Both approaches lead to Equation 17 as the representation of the process, in a single-step reaction. The presence of crystallization water was not considered, since the salt hydration degree varies with the temperature and with the crystallization conditions^{7,23}.

$$CaO + SiO_2 \rightarrow CaSiO_3$$
 (17)

According to Equation 17, the calcium oxide concentration reduces during the reaction, so it is expected that the medium pH reduces while the reaction proceeds, and then remains approximately constant when the limiting reactant is completely consumed.

In order to evaluate the consistency of this hypothesis, it is important to perform the integral analysis of the kinetic data. As extensively described by Levenspiel⁸, the integral method consists of integrating the kinetic expression proposed for a particular mechanism, and then comparing this theoretical curve of concentration varying with time with the experimental values.

If the proposed mechanism is correct, then there must be a satisfactory correspondence between the integral curve and the data obtained. Since the integral analysis is based on theoretical principles, the result provides strong evidence for supporting a particular reaction mechanism⁸.

Defining the chemical species A as CaO, species B as SiO_2 , and the ratio M as the relation between the initial concentration of CaO to the initial concentration of SiO_2 , it can be demonstrated that, if Equation 17 is correct, then the instant concentration of CaO is described by Equation 18⁸.

$$F(t) = \ln \frac{M - x_A}{M(1 - x_A)} = C_{AO}(M - 1)kt \qquad (18)$$

Equation 18 applicability is limited to the situations where $M \neq l$ and gives a linear plot when its left side, $\ln[(M-x_A)/M(1-x_A)]$, is graphically correlated with the reaction time. If the experimental data is satisfactorily fitted by the straight line described by Equation 18, the fitting angular coefficient is equals to $C_{A0}(M-1)k$. The adjusted curve usually shows a residual linear coefficient which is not related to the particular chemical kinetics but is due to random experimental errors⁸.

When using the methodology for the special case where M = 1, the expression which must be valid if Equation 17 is correct is the Equation 19. This expression gives a linear plot when its left side is graphically correlated with reaction time. Now, the angular coefficient is equals to k, and the linear coefficient is equals to $1/C_{A0}^{8}$.

$$\frac{1}{C_A} = \frac{1}{C_{AO}} + kt \tag{19}$$

Since there is significant difference depending on the value of M, experiments should be performed under conditions in which M = I, or in which M is significantly different from 1⁸. Then, the experiments in this study were performed under conditions in which $M \approx 0.25$.

The experiments are summarized in Table 2. Calcium oxide was chosen as the limiting reactant, since this would provide the highest variation in pH, enhancing the sensor sensitivity and allowing the correct detection of the reaction dynamics. Silica masses values were chosen in accordance with the following criteria: (1) the silica masses should be in large excess, but the value of M should be maintained constant, for providing a simpler integral analysis; (2) the masses or proportions of reactants should be in accordance to the values used in studies applying Chapelle test; (3) since one of the objectives of this research was to provide savings of energy and use of chemical reactants, the values should be as lower as possible, but sufficiently large for maintaining the sensor capability in detecting pH variations during the reactions.

3 Results and Discussion

3.1 Materials characterization

The three silica materials were analyzed by SEM technique in Brazilian Nanotechnology National Laboratory (LNNano) microscope (FEI Quanta 650 FEG, USA), and the particles dimensions were graphically evaluated using the Image Viewer application of MATLAB 2016 (Mathworks, USA), an image processing routine that is capable of performing the quantification and measurement of different objects and shapes in a particular image. The SEM samples were prepared by depositing the powder over a conductive carbon

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Experiment	SiO ₂ source	Temperature (°C)	Mass of CaO (g)	Mass of SiO ₂ (g)
Q1	Crystalline quartz	65	0.7168	3.0500
Q2	Crystalline quartz	75	0.6635	3.0010
Q3	Crystalline quartz	55	0.7355	2.2257
Q4	Crystalline quartz	80	0.7267	2.9967
Q5	Crystalline quartz	70	0.7018	3.0047
Q6	Crystalline quartz	70	0.7054	3.7558
NS1	Soot	70	0.7047	2.9901
NS2	Soot	60	0.6153	2.9956
NS3	Soot	65	0.7149	3.0183
NS4	Soot	75	0.7149	3.0053
AS1	Active silica	75	0.7032	3.0019
AS2	Active silica	65	0.6373	3.0172
AS3	Active silica	60	0.7105	2.9907
AS4	Active silica	70	0.7042	3.0069
AS5	Active silica	80	0.7031	3.0007
AS6	Active silica	70	0.7054	2.9985
AS7	Active silica	75	0.7213	3.7277

double-sided tape fixed in the stub. The samples were also carbon coated using a Bal-Tec SCD 050 Sputter Coater to obtain images under a high vacuum regime.

The XRD analyses were performed using a Rigaku DMAX 2200 diffractometer (Rigaku, Japan), with fine focus Cu tube ($\lambda = 1.54$ Å), Bragg-Bretano geometry (θ -2 θ), 0.02° step and 2.5 s/step exposition time.

The quartz particles, shown in Figure 4, presented nonspherical morphologies, with considerable dispersion in their average dimensions (Table 3), which was expected due to the comminution process^{21,24,25}.

According to the quartz XRD pattern, shown in Figure 5, the sample is comprised of practically α -quartz, with the absence of amorphous halo. This same figure also shows that active silica and soot are essentially amorphous, with a low-intensity crystalline peak near $2\theta = 20^{\circ}$.

The SEM images obtained for the soot and for the active silica are shown in Figure 6 and Figure 7, respectively, and indicate spherical particles with diameters in the range of nanometers (Table 3). Active silica particles also showed a broader diameter



Figure 4. SEM image obtained for crystalline quartz.

Table 3. Average diameters and sphericities of analyzed silica particles.

Material	Average particle diameter	Average sphericity	
Crystalline quartz	$(0.66\pm0.05)~\mu m$	0.68 ± 0.03	
Soot	$(110 \pm 5) \text{ nm}$	≈ 1	
Active silica	(243 ± 7) nm	≈ 1	

distribution in comparison to the soot, what is expected from the fact that the VAD process is capable of providing a finer control regarding the morphology of produced nanoparticles¹⁸.

3.2 Kinetic experiments

The experimental results are summarized in Table 4, which presents the reaction time, initial pH, the total pH variation observed, the total conversion of calcium oxide and the linear correlation coefficient, R², obtained for the application of Equation 18.

It is important to note that, after the mixture of the reactants, the system can experience a "dead-time", when no reaction is noticeable. This time must not be considered for the linear plot analyses, since the integral method is based on the assumption that the chemical reaction starts as soon as the reagents are put in contact⁸.

From Figures 8 to 10, it is possible to notice that the concentration of calcium oxide reaches a constant value in a relatively short time interval. In most of the reactions, the chemical process is not able to convert all of the CaO, and the medium is still alkaline after the end of the reaction. It proves that not all of the silica is in acidic form, being not able to react with the base dissolved in liquid medium.

The graphics show a classical pattern obtained when a chemical equilibrium is reached⁹. This fact is in accordance with the silica chemical properties, since the acidic characteristics of the silica are related to its superficial free silanol concentration^{26,27}, and the formation and consequently



Figure 5. XRD pattern obtained for submicron quartz. The inset shows the soot and the active silica low-intensity crystalline peaks.



Figure 6. SEM image obtained for soot particles.



Figure 7. SEM image obtained for active silica particles.

	Reaction time (min)		Total pH variation observed	Total conversion of CaO (%)	R ² obtained for linear adjust
Q1	220	11.657	1.179	99.7	0.9825
Q2	150	11.233	0.563	32.7	0.9615
Q3	130	12.005	0.395	100.0	0.9246
Q4	230	11.267	0.903	39.8	0.9422
Q5	200	11.333	0.510	54.1	0.9047
Q6	240	11.484	2.169	74.0	0.9746
NS1	30	11.957	0.936	100.0	0.8467
NS2	30	11.548	0.539	100.0	0.9088
NS3	120	11.100	0.296	31.2	0.9301
NS4	100	10.852	0.997	13.9	0.9048
AS1	80	11.546	2.072	81.8	0.9814
AS2	80	11.373	1.725	60.5	0.9799
AS3	50	11.817	2.142	100.0	0.9919
AS4	10	12.045	2.305	100.0	-
AS5	50	11.430	2.152	62.5	0.8992
AS6	80	11.436	2.109	66.6	0.9036
AS7	80	11.220	1.978	40.4	0.8972

Table 4. Summary of results obtained.



Figure 8. Kinetic experiments conducted with crystalline quartz as the silica source. The lines are guides for the eye

reactivity of this group is represented by a chemical equilibrium between silica and water^{26,27}. The consequence is that, depending on the particular conditions of the medium, not all of the silanols are able to react as acid groups, and such acid groups are in equilibrium with neutral groups^{26,27}.

It is important to realize that, when the reaction is complete, the system pH is considerably higher than 8, which is the approximate turning point of the phenolphthalein indicator at 25 °C¹⁰. It can be expected errors in the results for titrations if they are conducted at the same temperature of the reaction systems, higher than 25 °C, and it is also important to analyze



Figure 9. Kinetic experiments conducted with soot as the silica source. The lines are guides for the eye.



Figure 10. Kinetic experiments conducted with active silica as the silica source. The lines are guides for the eye.

if the equilibrium between the two different ionization states of the indicator¹⁰ is substantially affected by the temperature.

This variation would change the turning point, and a complete thermodynamic analysis would be necessary to verify if the equivalence point coincides with the indicator turning point¹⁰. Even if the titration temperature is rigidly controlled under 25 °C, the reversibility of the calcium oxide reaction can disturb the analysis since, according to Equations 3, 4 and 7, the species concentration in equilibrium can change with the variation of the temperature^{8,9}.

The solutions for Equations 3, 4 and 7 also show that, for temperatures higher than 55 °C, the neutral concentration of hydroxide ions is at least one order of magnitude higher than for 25 °C. The conclusion is that the neutral pH, where hydrogen and hydroxide ions concentrations are equal, is considerably higher than 7. As the Chapelle test does not consider this factor^{4,6}, one can expect several deviations between the "reactivity" calculated by this test and the real value of the reaction yield.

An accurate analysis of the results of the Chapelle test is difficult, since the medium temperature is increased until the aqueous solution reaches its bubble point^{4,6}. As the bubble point is a strong function of the local atmospheric pressure, and of the particular chemical species in the medium and their concentrations⁹, there is no standardization in the test temperature and, depending on all of these conditions, very specific reaction rates and equilibrium states will be obtained for the reaction^{8,9}. Since such factors change the observed yield, it will not be possible to compare results from different Chapelle test experiments, even when real experimental temperatures are documented.

The reaction times given in Table 4 are the time differences between the first instant when the concentration shows variation and the instant when the final *plateau* is reached, evidencing the end of the reaction. For each one of the three different silica sources, the mean values of the reaction times were evaluated with the ANOVA ("*analysis of variance*"). It is a statistical procedure for evaluating the confidence intervals of the mean results obtained for different samples and the significance of the differences between different means. If the confidence intervals show no intersections, it is possible to conclude with a given confidence - in this research, 95% confidence - that the mean results are statistically different.

Figure 11 shows the 95% confidence intervals of the mean reaction times observed for the crystalline quartz tests, for the soot tests, and for the active silica tests, obtained with the ANOVA test performed with 95% confidence, and Table 5 summarizes the values of the mean reaction times and the calculated confidence intervals. The analysis was performed in Minitab 17 (Minitab Inc, USA) and indicates a significant difference in the mean reaction time observed for crystalline quartz, which is considerably higher than the observed for the other silica sources, and no significant difference between the mean reaction times observed for active silica and for soot tests.



Figure 11. ANOVA test of the reaction times, with 95% confidence interval (CI) for mean reaction time. The lines connecting dots and the horizontal lines are guides for the eye.

In all of the experiments shown in Figure 8, there is an initial baseline before calcium oxide concentration varies significantly, and it is a determinant factor for the higher reaction time. As the silica amorphous materials have a lower

Table	e 5. M	lean re	eaction	times	and	95%	confic	lence	interva	ls ca	lcul	lated	d
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Silica source	Mean reaction time (min)	95% confidence interval for mean reaction time (min)			
Crystalline quartz	195.0	(161.1; 228.9)			
Soot	70.0	(28.4; 111.6)			
Active silica	61.4	(30.0; 92.9)			

reaction time, a feasible hypothesis is that the crystalline structure is responsible for the lower reaction rate.

It is possible that, before it is able to react with the free basic species dissolved in the liquid medium, the silica silanol groups must be exposed in the surface, and the rigidity of the crystalline structure reduces the number of available groups^{26,27}. Then, the initial baseline would be caused by the combined effect of the temperature, the electric interaction between the silica surface and the hydroxide negatively charged ions, and the liquid fluid dynamics.

These effects would be responsible for inducing the presence of silanol groups in silica surface, in accordance with the Zhuravlev model for silica chemistry²⁷. Then, the effective reaction only starts when there are sufficient acid groups able to neutralize the base.

Another important possibility is the effect of the surface area - it is a general principle in chemical kinetics that the reaction rate rises with the increase in surface area⁸.

Figures 4, 6 and 7 and the data presented in Table 3 evidence that the crystalline quartz shows a higher value of particle mean diameter, a lower value of sphericity and also has a lower specific surface area, what decreases the interaction area between the silica particles and the CaO, reducing the rate of reaction, according to the Langmuir theory⁸. The quantification of the adsorption sites on silica surface and the specific area of the particles needs a specific BET study⁸, and the analysis of this effect is an important limitation of the presented methodology. With the proposed instrumentation, it can only be performed qualitatively when there are available SEM images which evidence the differences in the specific area.

In most of the experiments conducted with soot and active silica, the reaction reaches the equilibrium *plateau* in a very short time, making it difficult to compare the results for different temperatures, since the temperature effect has little significance in these cases.

However, in quartz experiments, in which the time scale is wider, the tendency observed is in accordance with the hypothesis made. The initial reaction rate is increased with temperature, and both the Equation 17 and the analysis of Lux-Flood and Lewis theories suggest an acid-base neutralization reaction.

It is commonly observed that acid-base reactions are considerable exothermic⁷⁻¹⁰, and the chemical equilibrium in reactions with such thermodynamic behavior is favored by lower temperatures^{8,9}.

Figure 8 shows the correspondence between the total CaO converted and this hypothesized temperature behavior: the two lowest temperatures, 65 and 55 °C, show complete conversion; the two experiments conducted at 70 °C show a small variation, expected due to stochastic effects, and both cases show higher conversions than the other two experiments conducted in higher temperatures. The experiment performed at 75 °C exhibits a lower conversion than the experiment carried out at 80 °C. Finally, the experiment conducted at 80 °C, the highest temperature tested, shows the lowest total conversion of CaO.

Table 6 summarizes a comparison between the analyses performed with the methodology proposed in this research and the Chapelle test. It can be easily concluded that there are advantages related to time, energy consumed, and to more accuracy and confidence obtained in the experiments.

3.3 Mechanistic integral analysis

The fitting of the experimental values to the straight line described by Equation 18 was applied in order to verify if the kinetic data obtained was consistent with the proposed chemical mechanism. The linear correlation coefficient obtained for the adjusted straight lines were $R^2 \cong 1$ for all of the experiments, and this fact reveals a strong linear correlation and consistency with the hypothesis. It is worth noticing that the coefficient could not be calculated for experiment AS4 due to the low reaction time, since it is necessary to remove both the dead-time and the *plateau*, as it was already mentioned.

Figure 12 shows the straight lines F(t), defined by Equation 18, obtained for 4 experiments using crystalline quartz, and Figure 13 shows the straight lines obtained for 1 experiment using soot and for 2 experiments using active silica as the silica source.

The data show a complete agreement with the expected behavior, and it is possible to observe that some experiments for active silica obtained $R^2 > 0.98$, what is technically a perfect straight line. The deviations from the linear regression can be attributed to stochastic errors during the experiments.

The fitted straight lines F(t) obtained can be described by their angular and linear coefficients, and the angular coefficient is related to the kinetic rate constant k in each experimental temperature accordingly to Equation 18. Table 7 summarizes the coefficients obtained for each one of the linear adjustments, even the ones that were not shown in Figures 12 and 13, but the analysis could not be performed for experiment AS4 due to the low number of data collected. The main result showed in Table 7 is the consistency of the data, that show similar values and order of magnitudes for the same parameters. This data is important for reinforcing the kinetic hypothesis, a 1:1 reaction.

It is not possible to observe neither clear differences in the mean values of the parameters nor a tendency of the kinetic constants with the increase in the temperature range tested but, as

Table 6. Comparison between the proposed methodology and the Chapelle test⁴⁻⁶.

Kinetic and thermodynamic analysis proposed	Chapelle test
The analysis takes less than 3 hours.	The analysis takes 16 hours plus the time needed for the titration of the sample.
Energy and time savings, due to the use of less time and lower	The experimenter needs to heat the aqueous medium until its bubble
temperatures.	point and needs to maintain this temperature for 16 hours.

Procedure with more accuracy, more confidence, and more robustness, due to the use of electronic, simple and non-expensive equipment, without errors associated with visual procedures.

The analysis takes in account the composition of the medium and the temperature and pressure effects on the ionic equilibrium of water, allowing the comparison between experiments performed at different temperatures and different compositions of the medium.

of the entire kinetic behavior.

The analysis is done in situ, and all environmental effects are taken in account. There is no risk of disturbance in the chemical equilibrium due to the analysis procedure.

The procedure is fast, so the effects of parallel reactions with gases in atmospheric air are insignificant.

Kinetic experiments allow the quantification of interference caused by agents like: agitation power, solid-liquid equilibrium effects, reaction limitations by an increase in mass transfer resistance, and so on.

The methodology provides information on the intrinsic kinetic mechanisms, helping the elucidation of the phenomenon.

Lack of robustness to experimental errors. Sensitivity to visual errors, due to the use of colorimetric indicators in a turbid medium, and sensitivity to errors due to analyst's lack of experience in performing the titration.

The analysis does not take in account neither the temperature and pressure effects nor the effect of the differences in suspensions composition; such differences can change both the titration results and the bubble point temperature. Different Chapelle experiments cannot be compared, since the environmental temperatures are different. Chapelle tests are always performed with the same proportions, so the effect of the composition cannot be evaluated and chemical reactants cannot be saved.

Allows the observation of the presence of chemical equilibrium and Does not allow the observation of the dynamic behaviors, since consists in a single-point analysis.

> The sample must be carefully cooled to 25 °C for the titration procedure, due to the colorimetric agent equilibrium. This cooling process can change the apparent conversion, since the reversible reaction yield is dependent on the temperature.

> The experiment takes long time, 16 hours, and parallel reactions, such as the CaO neutralization by the air CO₂, can affect significantly the result.

> The analysis does not allow the evaluation of the interference caused by external effects, and all of the environmental parameters must be carefully controlled and kept constant.

> Chapelle test does not provide information about the intrinsic kinetic mechanism, providing no information about the phenomena involved.



Figure 12. Straight lines obtained for four of the experiments using crystalline quartz, in the integral analysis.



Figure 13. Straight lines obtained for one experiment using soot and for two experiments using active silica, in the integral analysis.

Experiment	Temperature (°C)	Angular coefficient of the linear regression	Linear coefficient of the linear regression	Numerical value of kinetic rate constant k obtained	R ² obtained for linear adjust
Q1	65	4.52 x 10 ⁻⁵	-5.49	1.20 x 10 ⁻³	0.9825
Q2	75	1.81 x 10 ⁻⁵	-6.09	5.13 x 10 ⁻⁴	0.9615
Q3	55	8.74 x 10 ⁻⁶	-2.93	2.61 x 10 ⁻⁴	0.9246
Q4	80	1.07 x 10 ⁻⁵	-5.20	2.70 x 10 ⁻⁴	0.9422
Q5	70	2.13 x 10 ⁻⁵	-5.55	5.79 x 10 ⁻⁴	0.9047
Q6	70	1.49 x 10 ⁻⁵	-7.97	3.78 x 10 ⁻⁴	0.9746
NS1	70	3.27 x 10 ⁻⁴	-5.46	8.88 x 10 ⁻³	0.8467
NS2	60	3.93 x 10 ⁻⁴	-6.89	1.16 x 10 ⁻²	0.9088
NS3	65	1.64 x 10 ⁻⁵	-5.41	4.39 x 10 ⁻³	0.9301
NS4	75	6.30 x 10 ⁻⁶	-5.37	1.61 x 10 ⁻⁴	0.9048
AS1	75	9.05 x 10 ⁻⁵	-5.51	2.34 x 10 ⁻³	0.9814
AS2	65	1.64 x 10 ⁻⁴	-6.58	4.56 x 10 ⁻³	0.9799
AS3	60	1.79 x 10 ⁻⁴	-5.38	4.80 x 10 ⁻³	0.9919
AS4	70	-	-	-	-
AS5	80	4.96 x 10 ⁻⁵	-5.51	1.28 x 10 ⁻³	0.8992
AS6	70	1.68 x 10 ⁻⁵	-5.47	4.55 x 10 ⁻⁴	0.9036
AS7	75	2.95 x 10 ⁻⁵	-7.60	7.40 x 10 ⁻⁴	0.8972

Table 7. Angular and linear coefficients of Equation 18 and numerical values of the rate constants obtained for each experiment.

it was already cited, a complete study of the correlation between kinetics and the specific surface area should be performed in future works in order for determining possible correlations.

4. Conclusions

The integral analysis provided semi-empirical evidence for the proposed mechanism, a 1:1 reaction, since it is very unusual for a chemical reaction to agree with more than one integral straight line⁸, and the satisfactory adjustment to the proposed model was obtained for 16 experiments performed under different conditions. It is important, however, to emphasize that, due to the very small scales of dimensions and time events, it is very difficult to prove that a particular mechanism is valid for generalized cases, since the events take place in the molecular and atomic levels⁸. A proposed mechanism can be accepted as a right and consistent one until unquestionable facts against it have been discovered⁸.

The statistically significant difference of mean reaction times obtained for different silica sources provided evidence that the crystalline structure and the particles specific surface area can be determinant factors for the reaction rates, and these hypotheses are supported by the silica model developed by Zhuravlev²⁷ for the chemistry of silanol groups in water, and by the Langmuir kinetic model⁸, respectively. It was verified a reaction time of 195 min for crystalline silica particles with average diameter of 0.66 μ m, and reaction time of 61 min for active silica particles with average diameter of 243 nm. Both reaction times are very lower than the standard time of the Chapelle test, 16 hours plus the time required for the titration chemical analysis.

It is important to realize that the proposed analysis has many advantages in comparison to the traditional Chapelle test. Besides the less time and energy-consuming, the procedure prevents the analysis to be affected by parallel reactions, such as the reaction with carbon dioxide from atmospheric air, and takes in account the effects of the temperature, allowing the comparison between experiments performed in very different conditions, since the reaction parameters are corrected by rigorous thermodynamic equations. It is also able to eliminate the imprecisions related to the visual titration technique, that can show unsatisfactory results in excessive turbid media, and the fluctuations related to the poor temperature control. It is possible to evaluate the temperature effects on the reversibility of the reaction as well, but there is an intrinsic limitation in evaluating the effect of the particles surface area, which needs a separate BET study.

The next studies should then evaluate the specific surface area effect on chemical reaction rate and evaluate if temperatures even lower than 55 °C can be employed for the analysis, depending on the granulometry, providing even more energy savings and helping the elucidation of

the effects of the surface energy on interactions between nanoparticles.

The titration with chemical indicators which change their colors in the turning point - used in Chapelle test - is a classic analytical procedure, but it is particularly sensitive to the analyst experience and familiarity with the technique¹⁰. In this sense, the use of an electronic, simple and non-expensive device, such as the pH meter, provides more accuracy and confidence to the results obtained and important time savings, being more robust in relation to the possible errors of the experimenters.

5. Acknowledgements

The authors would like to thank Brazilian Nanotechnology National Laboratory LNNano) for the use of the facilities, CNPq, CAPES, and FAPESP Grants 2015/02185-3 and 2017/20445-8 for financial support.

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