

# Microstructure and Mechanical Properties of Thermal Sprayed Nanostructured Cr<sub>3</sub>C<sub>2</sub>-Ni20Cr Coatings

*Cecilio Alvares da Cunha, Nelson Batista de Lima, Jose Roberto Martinelli, Ana Helena de Almeida Bressiani\*, Armando Guilherme Fernando Padial, Lalgudi Venkataraman Ramanathan\**

*Instituto de Pesquisas Energeticas e Nucleares – IPEN,  
Av. Prof. Lineu Prestes 2242, Cidade Universitaria  
05508-000 São Paulo - SP, Brazil*

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Cr<sub>3</sub>C<sub>2</sub>-Ni20Cr coatings have been used for corrosion and wear resistant applications. However, one of the shortcomings of these coatings is its low hardness, and consequent low wear resistance, for long term high temperature applications. Nanostructured coatings of many materials have exhibited higher hardness and strength compared with conventional coatings of the same material. Consequently, nanostructured coatings of other materials, including Cr<sub>3</sub>C<sub>2</sub>-Ni20Cr have been attempted to enhance overall performance. In this study the effects of high energy milling parameters on Cr<sub>3</sub>C<sub>2</sub>-25(Ni20Cr) powder characteristics as well as the microstructure and mechanical properties of nanostructured Cr<sub>3</sub>C<sub>2</sub>-25(Ni20Cr) coatings formed by high velocity oxygen fuel (HVOF) spraying have been evaluated. The average particle size and crystallite size of milled Cr<sub>3</sub>C<sub>2</sub>-25(Ni20Cr) powders decreased with increase in milling time and this decrease was more pronounced in nitrogen compared to that in hexane. This difference has been attributed to a cushioning effect in the latter medium. The coatings prepared with milled Cr<sub>3</sub>C<sub>2</sub>-25(Ni20Cr) powders had a more uniform microstructure, were harder and had higher relative fracture toughness compared with coatings prepared with as-received powders.

**Keywords:** *Chromium carbide, nanostructured coating, mechanical milling, thermal spraying*

## 1. Introduction

Coatings containing chromium carbide particles distributed in a nickel-chromium alloy matrix (Cr<sub>3</sub>C<sub>2</sub>-NiCr system) have been used for corrosion and wear resistant applications. These coatings can be used in corrosive environments at temperatures (up to 900 °C), much higher than that at which the harder WC-Co coatings can be used. The latter undergo decarburization to W<sub>2</sub>C or to W upon extended exposure to high temperatures and to degradation of mechanical properties<sup>1,2-5</sup>. However, one of the shortcomings of Cr<sub>3</sub>C<sub>2</sub>-NiCr coatings is its lower hardness and lower wear resistance, compared to WC-Co coatings<sup>6</sup>. This has led to attempts at producing nanostructured Cr<sub>3</sub>C<sub>2</sub>-NiCr coatings for improved hardness and overall performance. During the last decade, thermal sprayed coatings of various materials prepared with nanocrystalline feed stock have exhibited higher hardness, strength and corrosion resistance compared to those prepared with conventional feed stock powders of the same materials<sup>7-10</sup>. Several methods have been used to prepare thermal sprayed nanostructured coatings. These include direct spraying of nanosized powders with or without gaseous or liquid precursors and also spraying of specially designed alloys with low critical cooling rates<sup>11-14</sup>. In the latter method, upon spraying, the alloys with low critical cooling rates become amorphous, and the coating is then devitrified by heating<sup>10,14</sup>. The most widely used method consists of high energy mechanical milling of conventional powders to obtain nanocrystalline powders, which are subsequently agglomerated to the required size prior to spraying<sup>15-20</sup>.

Mechanical milling enables large quantities of nanostructured materials to be produced and during milling the powder grains are continuously refined by cold welding and fracturing<sup>21-24</sup>. Nanostructured composites consisting of hard particles and a metal binder, such as Cr<sub>3</sub>C<sub>2</sub>-NiCr or WC-Co, have been prepared by mechanical

milling<sup>5,25,26</sup>. Milling of Cr<sub>3</sub>C<sub>2</sub>-NiCr has been done in a variety of environment. The environment contributes mainly to reduction of contaminants in the powders, to control powder temperature and to control powder characteristics. The milling environment could be gaseous (argon, nitrogen, hydrogen), liquid (liquid nitrogen, acetone, hexane) or solid (stearic acid)<sup>26</sup>. Powders of Cr<sub>3</sub>C<sub>2</sub>-NiCr have been milled mainly in liquid hexane [H<sub>2</sub>C(CH<sub>2</sub>)<sub>4</sub>CH<sub>3</sub>]<sup>26</sup>. Data about milling of Cr<sub>3</sub>C<sub>2</sub>-NiCr powder in gaseous nitrogen is scarce. This paper presents and compares the effects of high energy mechanical milling of Cr<sub>3</sub>C<sub>2</sub>-25(Ni20Cr) powder in liquid hexane and gaseous nitrogen. The influence of milling time on Cr<sub>3</sub>C<sub>2</sub>-25(Ni20Cr) powder characteristics as well as the microstructure and mechanical properties of nanostructured Cr<sub>3</sub>C<sub>2</sub>-25(Ni20Cr) coatings prepared using high velocity oxygen fuel (HVOF) spraying of the milled powders are also presented.

## 2. Materials and Methods

### 2.1. Milling of powders

Conventional Cr<sub>3</sub>C<sub>2</sub>-25(Ni20Cr) powders with average particle size of 25 μm were used in this study. These powders were milled for 1, 2, 4, 8 and 16 hours in a ZOZ high energy mill at 400 rpm and with ball-to-powder ratio of 10:1. Milling was done in two different media, liquid hexane and gaseous nitrogen. The particle size, grain (crystallite) size and phase constituents of the milled powders were determined as a function of the milling medium and duration. A CILAS particle size analyzer was used to determine the average particle size and a scanning electron microscope (SEM) coupled to an energy dispersive system (EDS) was used to examine particle morphology

\*e-mail: abressia@ipen.br, lalgudi@ipen.br

and determine its composition. X ray diffraction (XRD) analysis of the as-received and milled powders was carried out to determine the crystallite sizes. The main peak of  $\text{Cr}_3\text{C}_2$  in the diffraction pattern, in conjunction with the Scherrer Equation 1 was used to determine the average crystallite size of the powders<sup>27,28</sup>. This equation relates crystallite size (D) and the full-width at half-maximum (FWHM), referred to as  $\Delta(2\theta)$  of XRD reflections.

$$D = 0.9\lambda / \Delta(2\theta) \cos\theta \quad (1)$$

where  $\lambda$  is the wavelength (in the case of a Cu target,  $\lambda = 0.15406$ ) and  $\theta$  is the diffraction angle. The use of this equation is based on the physical origin of broadening of the XRD reflections being associated with the small grain size only. The true peak broadening  $\Delta(2\theta)$  can be obtained using Equation 2:

$$\Delta(2\theta) = [(\Delta(2\theta)_h)^2 - (\Delta(2\theta)_g)^2]^{1/2} \quad (2)$$

where  $\Delta(2\theta)_h$  is the FWHM of the measured profile and  $\Delta(2\theta)_g$  is the FWHM of the profile from the standard sample for the same reflection. The grain size thus obtained is volume averaged in a direction perpendicular to the diffraction plane.

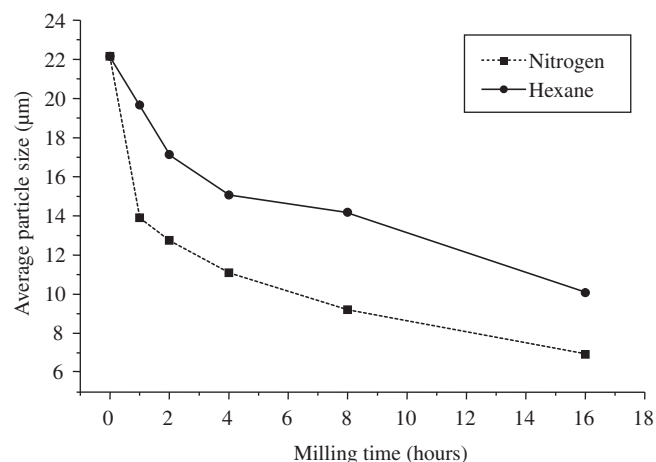
## 2.2. Thermal sprayed coatings

The  $\text{Cr}_3\text{C}_2$ -25(Ni20Cr) powder in the as-received condition and that milled for 4 hours in nitrogen were used as feed stock for thermal spraying coatings on AISI 310 specimens  $50 \times 20 \times 2$  mm using the high velocity oxygen fuel (HVOF) process. The average particle size of the milled powders was  $11 \mu\text{m}$ , close to the lower limit of acceptable particle sizes for HVOF spraying. The average coatings thickness was  $200 \mu\text{m}$ . The spraying parameters and gun to specimen distance were identical while spraying the two types of powders. The microstructure and phase composition of the coating cross-sections were examined and determined respectively, with a SEM/EDS system. The hardness of the coatings was determined across its sections, using loads of 500 and 1000 g. The average hardness was determined from five indentations in the middle of each of the coating sections, away from the two interfaces.

## 3. Results and Discussion

### 3.1. The milled powders

Figure 1 shows the variation in average particle size of  $\text{Cr}_3\text{C}_2$ -25(Ni20Cr) powders as a function of milling time in hexane and in



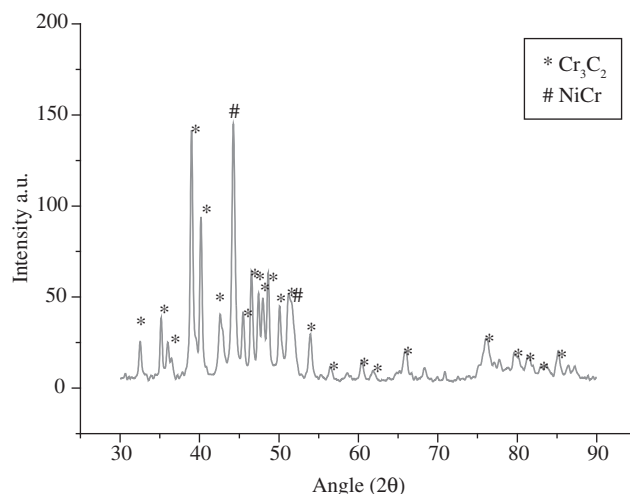
**Figure 1.** Effect of milling medium and duration on  $\text{Cr}_3\text{C}_2$ -25(Ni20Cr) powder particle size.

gaseous nitrogen. In the two milling media, the average particle size decreased with increase in milling time. The decrease in average particle size with milling time in nitrogen was significant compared to that in hexane. Reductions in  $\text{Cr}_3\text{C}_2$ -25(Ni20Cr) powder particle size to  $5 \mu\text{m}$  upon milling in hexane have been reported<sup>5,26</sup>. However, in this study the particle size of powders milled for the same duration in hexane was only  $10 \mu\text{m}$ . The marked reduction in particle size of powders milled in nitrogen compared to that milled in liquid hexane as well as the differences in the particle size of powders milled in hexane for similar duration, between that reported<sup>5,26</sup> and in this study was further investigated. This consisted of measuring the particle and crystallite sizes of  $\text{Cr}_3\text{C}_2$ -25(Ni20Cr) powders milled separately for 8 hours with 10, 50 and 100 ml of liquid hexane in the ZOZ mill. In these measurements, the amount of powder and other milling parameters were maintained identical. Particle size variations as a function of hexane volume are shown in Table 1. Significant decrease in particle size with reduction in the amount of hexane indicate a cushioning effect in liquid hexane compared to that in nitrogen as the milling medium in the initial experiments.

X ray diffraction patterns of the milled powders were used to determine the crystallite sizes. Figure 2 shows a typical diffraction spectrum of  $\text{Cr}_3\text{C}_2$ -25(Ni20Cr) powder milled in nitrogen. The diffraction peaks were identified and the  $\text{Cr}_3\text{C}_2$  reflection at  $2\theta \approx 39^\circ$  was used to determine the crystallite size with the Scherrer Equation 1 mentioned earlier. Aware that micro-deformation and instrument and/or measurement conditions also affect peak broadening, Figures 3a and 3b were plotted. Figure 3a reveals fitting of the Gaussian curve, corresponding to micro-deformation, and Figure 3b, the fitting of the Lorentzian curve, attributable to crystallite size on the selected peak in the diffraction pattern. The peak profile can be seen to be mainly Lorentzian, indicating that peak broadening was due to crystallite

**Table 1.** Effect of hexane volume on average particle size of milled  $\text{Cr}_3\text{C}_2$ -25(Ni20Cr) powders.

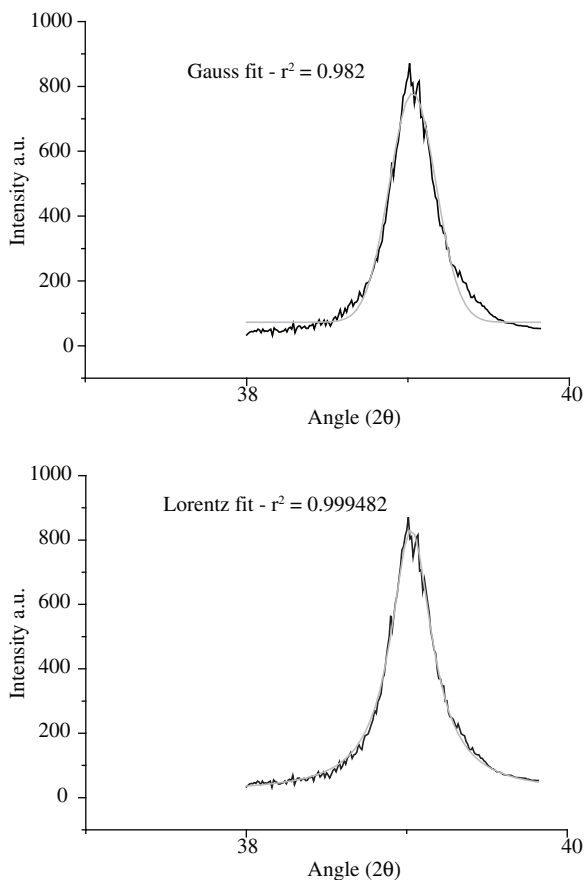
$\text{Cr}_3\text{C}_2$ -25(Ni20Cr) powder	Average powder particle size ( $\mu\text{m}$ )
As received	35.79
Milled with 100 mL hexane	10.00
Milled with 50 mL hexane	5.00
Milled with 10 mL hexane	2.60



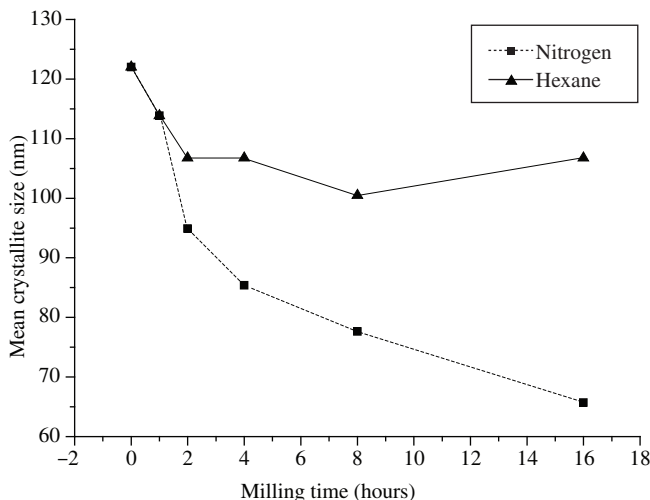
**Figure 2.** X ray diffractogram of  $\text{Cr}_3\text{C}_2$ -25(Ni20Cr) powder milled for 8 hours in nitrogen.

size. The average crystallite size of the particles was determined using the Scherrer Equation 1 after subtracting for peak broadening due to the instrument. This technique permits measurement of average crystallite sizes of up to 150 nm<sup>27</sup>.

The average crystallite size of Cr<sub>3</sub>C<sub>2</sub> in the milled powders decreased with increasing milling time as shown in Figure 4. The aver-



**Figure 3.** a) Gaussian fit and b) Laurentzian fit on the main Cr<sub>3</sub>C<sub>2</sub> peak of the diffraction spectrum of Cr<sub>3</sub>C<sub>2</sub>-25(Ni<sub>20</sub>Cr) powder milled for 8 hours in nitrogen.



**Figure 4.** Average crystallite size of Cr<sub>3</sub>C<sub>2</sub>-25(Ni<sub>20</sub>Cr) powder as a function of milling medium and milling time.

age crystallite size decreased from 125 nm to 65 nm after 16 hours of milling in nitrogen. The reduction in average crystallite size of Cr<sub>3</sub>C<sub>2</sub> as a function of milling time in hexane was less and this could be also attributed to the cushioning effect of the liquid hexane, as corroborated by data shown in Table 2 in which crystallite size decreases with decrease in the volume of hexane in the mill.

The as-received and milled powders were examined in the SEM. Microscopic features, other than powder sizes were similar in both the as-received and the milled powders. The Cr<sub>3</sub>C<sub>2</sub> particles were embedded in the Ni-Cr alloy phase. Figures 5a and 5b reveal micrographs of the powders milled in nitrogen for 4 hours. Figure 5b is a higher magnification micrograph of a region in Figure 5a. The energy dispersive spectrum shown in Figures 5c and 5d are of the dark and light regions in the powder particle shown in Figure 5b. The dark regions with 95 at % Cr were Cr<sub>3</sub>C<sub>2</sub> particles and the light regions, the Ni-Cr alloy phase.

### 3.2. The HVOF sprayed coatings

The microstructures of cross-sections of coatings prepared with as-received and milled Cr<sub>3</sub>C<sub>2</sub>-25(Ni<sub>20</sub>Cr) powders are shown in Figure 6. The coating with the milled powder (nanostructured coating) contained fewer pores, was more uniform and dense as shown in Figures 6c and 6d, compared to the coating prepared with as-received powders that are shown in Figures 6a and 6b. The higher magnification micrographs in Figures 6b and 6d are of regions shown in Figures 6a and 6c. The very bright regions in the micrographs in Figures 6a and 6c are contaminants. The light, light grey and dark grey regions (shown with arrows) were analyzed using EDS in the SEM. This analysis revealed large Ni peaks and very small Cr peaks (similar to that shown in Figure 5c) on the light region indicating it to be the Ni-Cr alloy phase. The dark grey regions rendered large Cr peaks in the EDS spectrum indicating it to be the Cr<sub>3</sub>C<sub>2</sub> phase. The light grey regions contained the two phases, Cr<sub>3</sub>C<sub>2</sub>, Ni-Cr, indicating it to be a composite phase. Similar observations have been reported<sup>29</sup>.

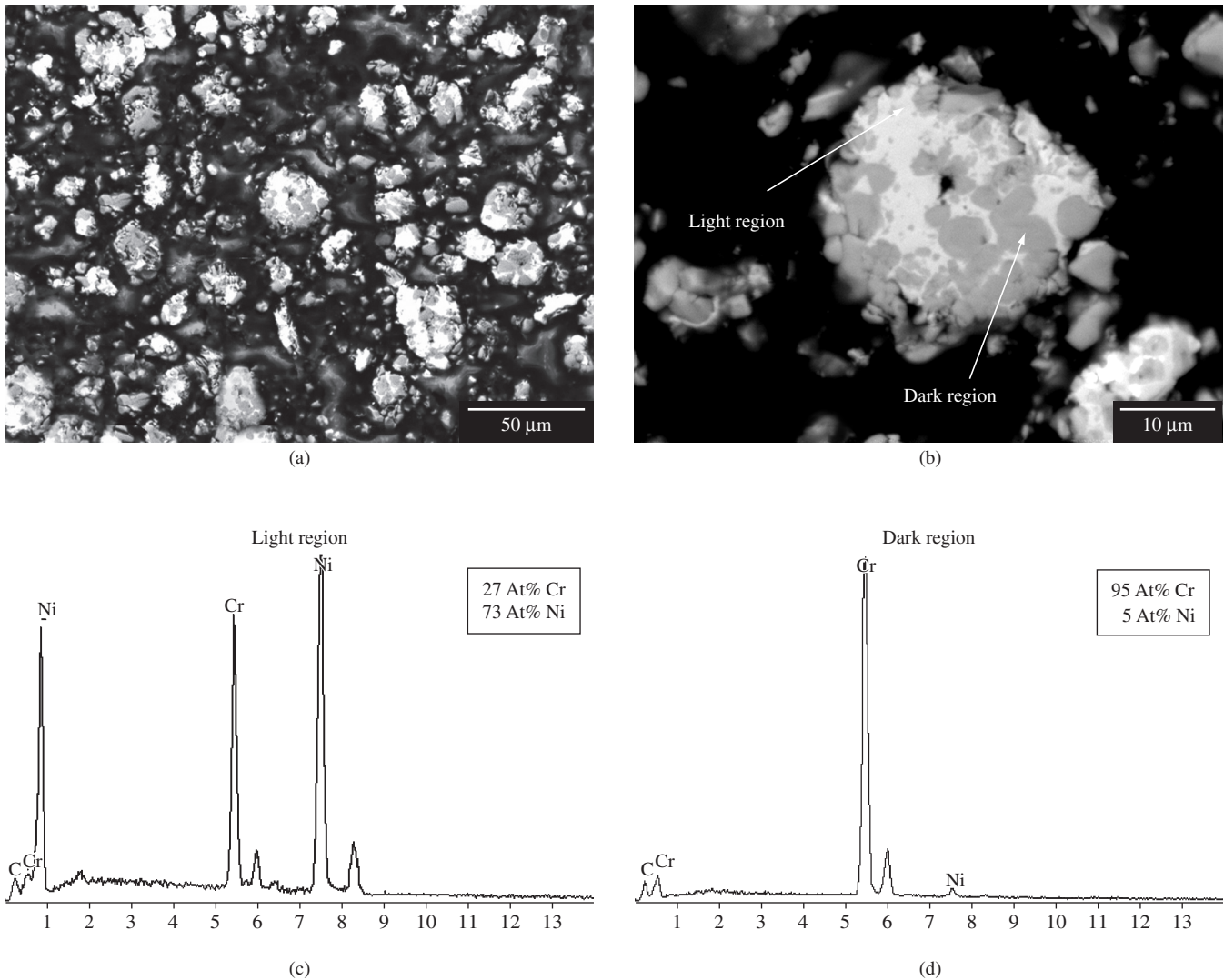
The hardness test data are shown in Table 3. The hardness of the nanostructured coatings was higher than that of the coatings with as-received powders. Cracks emanating from the indents were observed in the two types of coatings and are indicated in the micrographs of Figure 7. The cracks seen in the coatings obtained with the as-received powders were longer and wider. The cracks in both types of coatings were mainly parallel to the substrate. Similar findings have been reported<sup>5,10</sup>. The crack lengths were used to qualitatively compare

**Table 2.** Effect of hexane volume on average crystallite size of milled Cr<sub>3</sub>C<sub>2</sub>-25(Ni<sub>20</sub>Cr) powder.

Cr <sub>3</sub> C <sub>2</sub> powder	Average crystallite size (nm)
As received	78
Milled with 50 mL of hexane	54
Milled with 10 mL of hexane	49

**Table 3.** Microhardness of HVOF coatings with as-received and nanocrystalline Cr<sub>3</sub>C<sub>2</sub>-25(Ni<sub>20</sub>Cr) powder.

	Hardness of HVOF coatings with	
	As-received powder	Nanocrystalline powder
Coating thickness (μm)	190	214
500 g load	810.0 ± 34.51	1124.5 ± 208.6
1000 g load	795.0 ± 13.35	1062.5 ± 64.35



**Figure 5.** a, b) Scanning electron micrographs of  $\text{Cr}_3\text{C}_2\text{-25(Ni20Cr)}$  powder milled for 4 hours in nitrogen; c, d) EDS of light and dark regions in the large particle seen in b) indicating these to be the Ni-Cr alloy and  $\text{Cr}_3\text{C}_2$  respectively.

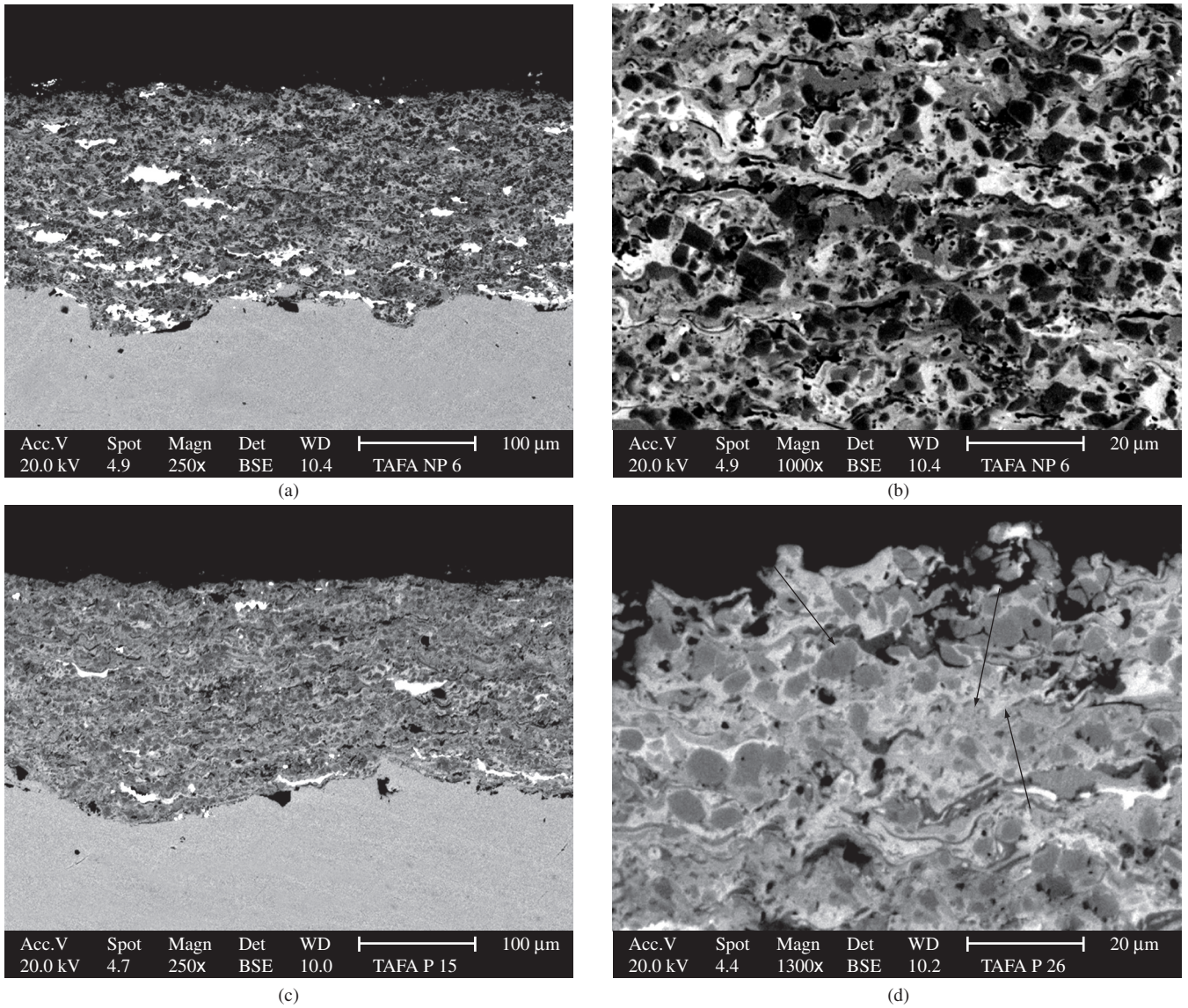
the fracture toughness of the coatings prepared with as-received and milled powders. This comparison was based on reported linear correlations between hardness and resistance to cracking in these types of coatings<sup>7</sup>. This indicated that the relative fracture toughness of the nanostructured coating was higher. Some of the cracks were along the phase boundaries in the coatings. There were fewer cracks in the nanostructured coating, due probably to composite formation and higher hardness.

#### 4. General Discussion

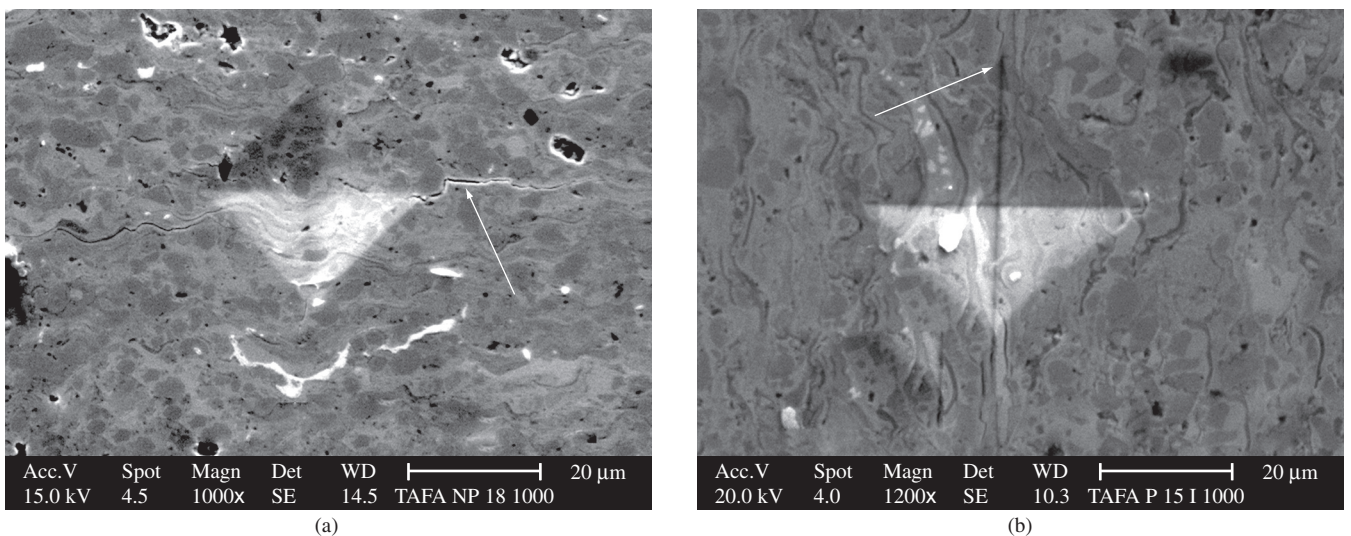
The hardness of thermal sprayed coatings is affected by the technique as well as characteristics of the feed stock<sup>2,3,30,31</sup>. In the HVOF technique, the particle velocity is high and thermal energy low, and this leads to high hardness<sup>32</sup>. It has been reported that nanostructured materials often exhibit higher hardness compared to corresponding conventional materials, although lower than that predicted using the classical Hall-Petch equation<sup>33-35</sup>. In this investigation also the hardness of nanostructured  $\text{Cr}_3\text{C}_2\text{-25(20NiCr)}$  coating was higher than that of the coating prepared with as-received powders. The higher hardness of the nanostructured coatings is considered to be due to

the uniform microstructure caused by the mechanical milling process to obtain feed stock and the intrinsically high hardness of the nanostructured material.

The indentation fracture method has been used to obtain information about the relative fracture toughness of coatings<sup>29</sup>. In this study, at 1000 g hardness test load, cracks emanating from the indents were observed in both types of coatings. These cracks were mostly parallel to the coating surface and were not present directly on the extended line of the diagonal of the indentation. Many indentation cracks were also observed along the carbide - metal binder interface in coatings prepared with the as-received powder. (Figure 7) Fewer indentation cracks were observed in the nanostructured coatings at the same hardness test load. These results indicated that crack propagation within the coating had a preferred direction and there was high resistance to indentation fracture in the direction perpendicular to the coating surface. The preferred direction for crack propagation could be attributed to the thermal spray process. A complete coating is produced by passing the spray torch many times across the substrate and this could result in contamination of a deposited layer prior to deposition of the next layer. Also differences in the thermal expansion



**Figure 6.** Cross-sections of HVOF coatings: a) and b) with as-received Cr<sub>3</sub>C<sub>2</sub>-25(Ni<sub>20</sub>Cr); c) and d) nanostructured Cr<sub>3</sub>C<sub>2</sub>-25(Ni<sub>20</sub>Cr).



**Figure 7.** Typical microhardness indents with 1000 g load and cracks (arrows) emanating from the indents on cross-sections of HVOF coatings of Cr<sub>3</sub>C<sub>2</sub>-25(Ni<sub>20</sub>Cr): a) with as-received powder; b) with powder milled for 4 hours in nitrogen.

coefficient between the carbide and alloy phases could contribute to crack propagation along the phase interface. Discontinuity in heat and mass transfer has also been cited to result in discontinuity in the coating along which cracks propagate<sup>29</sup>. Indents associated with the lower hardness test load of 500 g revealed few cracks in the coating prepared with as-received powders, and none in the nanostructured coating. These observations suggest that the nanostructured coating possesses a higher resistance to cracking or higher apparent fracture toughness relative to that of the coating prepared with as-received powders. Since abrasion resistance of a coating is related to the apparent fracture toughness, it is evident that the nanostructured Cr<sub>3</sub>C<sub>2</sub>-25(Ni20Cr) coatings have higher abrasion resistance<sup>36</sup>.

## 5. Conclusions

- High energy milling of Cr<sub>3</sub>C<sub>2</sub>-25(Ni20Cr) powders in gaseous nitrogen and liquid hexane reduced the average particle size. The reduction in particle size with increase in milling time was more pronounced in nitrogen compared with that in liquid hexane.
- The average crystallite size of the milled Cr<sub>3</sub>C<sub>2</sub>-25(Ni20Cr) powders also decreased with increase in milling time. The average crystallite size reduction was significant in powders milled in nitrogen.
- Insufficient particle and crystallite size reductions in liquid hexane, compared to that in gaseous nitrogen are attributed to a cushioning effecting in liquid hexane.
- The microstructure of HVOF sprayed coatings of Cr<sub>3</sub>C<sub>2</sub>-25(Ni20Cr) prepared with milled powders was uniform compared with those prepared with as-received powders.
- The hardness and fracture toughness of the nanostructured Cr<sub>3</sub>C<sub>2</sub>-25(Ni20Cr) coatings were higher compared with coatings prepared with the as-received powders.

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