Gamma Ray and FTIR Studies in Zinc Doped Lead Borate Glasses for Radiation Shielding Application

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Gamma ray shielding properties of borate glass samples containing oxides of lead and zinc are prepared by melt and quench technique and evaluated theoretically using XCOM computer software for gamma ray shielding properties. However, gamma ray shielding properties are discussed in terms of various calculated parameters such as half value layer, mean free path and mass attenuation coefficient. The calculated parameters are compared by the author with conventional shielding material concrete. FTIR studies are undertaken to investigate the various structural groups present in the prepared system. Furthermore, it was observed that the glass sample S1 posses minimum HVL value and maximum mass attenuation coefficient, It has been inferred that addition of lead improve the gamma ray shielding properties and simultaneously decrease the rigidity of the glass systems due to formation of non bridging oxygen. Gamma ray shielding properties of our glass systems have been compared with standard nuclear radiation shielding concrete.

Keywords: glass, FTIR, mass attenuation coefficients, mean free path, half value layer.

1. Introduction

Recent advancement of nanotechnology has made nanoscience hot area of research due to their infinite number of advantageous properties. Beside, the focused have been made on gamma ray radiation for different purposes, including nuclear reactor, medicine, industries and nuclear power plant. In recent years transition metal oxide glasses have attracted greatly the attention of many researchers and industries because of their valuable optical and electrical properties¹. Heavy metal glasses containing boron oxide (B_2O_3) as a glass former are of great technological importance because of their wider range of their applications².

These glasses find their use in various applications including lightening, laboratory, cookware, medical, LCD screens and glass wool for thermal and acoustic insulation³. Borosilicate glasses containing lead is of great importance because it possesses desirable electrical resistivity, low melting points, high chemical stability over a wider range of concentrations⁴. Furthermore, these glasses play vital role in wide area of research and industrial applications related

to enamels, solder glasses, semiconductor microelectronics glass, ceramic cements and in nuclear waste immobilization⁵.

In recent time, the study of borate glass in particular, as one the major essential glass former, once it incorporated with certain amount of heavy metal such as lead oxide and zinc oxide its properties such as hardness, mechanical strength, transparency and optical properties, drastically change (4, 5). These B_2O_3 glasses is one of the form major glass former due to its higher bond strength, that make them promising candidate for feature shielding materials.

Usually, concrete are used as conventional shielding materials for protection of gamma radiations but due to certain limitations in the concrete like zero visibility and degradation of their mechanical strength in harsh environmental conditions, researchers requires some alternative method to replace it with another material with higher transference, mechanical strength and non-degradable⁶. Nowadays, borate and silicate glasses containing heavy metals becoming promising candidates as a radiation shielding materials.

The aim of present work is to investigate radiationshielding properties of some lead and Zinc based glasses and their structural properties using FTIR investigations.

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2. Experimental and Theoretical Techniques

All the synthesis chemical reagent of the glass was analytic grade used without further purification. The shielding glass sample was prepared via assisted melt quenching method as followed. A number of Pb₃O₄, ZnO, and H₃BO₃ were thoroughly mixed together. The homogenous mixture was subsequently place in the furnace for a period of 2h at 800 °C. The melt glass samples were rapidly cooled to room temperature. The glass sample's density was calculated using Archimedes principal benzene solution are used as immersion liquid. Furthermore, the molecular structure of the glass matrix were analyzed using Fourier Transformation Infrared spectrum (FTIR) (Perkin Elmer Spectrum 100 FTIR spectrometer)

The mass attenuation coefficient of the prepared glass samples have been investigated theoretically using Win XCOM computer software at different energies, and compare with standard shielding materials concrete ^{7,8}.

Molar volume (V_m) volume of the glass samples has been estimated by using the following expression:

$$V_{\scriptscriptstyle m} = M/\rho \tag{1}$$

Where ρ is the density of the sample and M is the molecular weight of the sample. The mass attenuation coefficients calculated using the equation (1)

$$\mu_m = \sum_{i}^n w_{i(\frac{\nu}{\rho})} \tag{2}$$

Where w_i is the weight and (μ/ρ) is the mass attenuation coefficient of the sample. The (μ/ρ) values can be taken directly from XCOM software or user-friendly Win XCOM software after substituting the sample composition. The linear attenuation coefficient (in cm⁻¹) is multiplication of $\mu_m = (\mu/\rho)$ value and density of the glass. One the easiest technique to determine the effectiveness of material toward the radiation shielding is to employ the idea of half value layer (HVL). This concept was defined by many researchers as the quantity of radiation shielding material needed to reduce the radiation intensity to one-half of the unshielded valve⁷.

$$HVL = (0.693/\mu)$$
 (3)

Where μ represent the linear attenuation coefficient and it can be found in the tabular form of radiation shielding parameter. In order to determine the attenuated energy phone in the absorbing medium, the Mean free path (MFP) was estimated as the distance in which the initial photon intensity can be reduced by 1/e factor. Therefore, mean free path (MFP) is considered as the reciprocal of the linear attenuation coefficient.

$$(MFP) = (1/\mu) \tag{4}$$

3. Result and Discussion

3.1 Densities and molar volume

The molar volume of the glass samples was calculated using equation 1. However, Table 1 contains the chemical composites of the prepared glass samples, densities and molar volume. Furthermore, it was observed that the density of the glass sample increases with increase of heavy metal content (lead oxide), the molar volume of the glass samples also increases with increase in concentration of these heavy metal oxides. The molar volume clearly shows that the prepared glass sample's structure corresponding to higher lead composition is becoming more open leading the formation of non-bridging oxygen⁹. The molar volume and density the glass samples corresponding to low lead compositions decreases due to decreases of heavy metal content.

3.2 Mean free path and mass attenuation coefficient

The estimated values of men free path (MFP) for all the samples are given in Table 2. From Table 2 it can be concluded that sample S4 has the lowest mean free path at high energy, which means the rate at which the photon energy is penetrating the sample is less in samples S4. Furthermore, the values of mean free path increase with the increase in the energy of incident Photon¹².

The glass samples were effectively prepared and its mass attenuation coefficient was evaluated using equation 2, and the results were given in the Table 3, at the energy ranging

Table 1. Composites chemicals, density (ρ) , molar volume (vm)

Name of Sample	Co	mpositio	ons	Sample	Molar Volume (cm³/mol)			
	PbO	ZnO	B ₂ O ₃	Density (g/ cm³)				
S1	20	0	80	3.75	26.75584			
S2	10	0	90	3.39	25.06729			
S3	5	5	90	3.35	23.25004			
S4	0	10	90	3.25	21.78373			

Table 2. Theoretical Result of Mean Free Path

	Mean Free Path (cm)									
Energy	S1	S2	S3	S4						
1.00E-03	6.3E-05	7.43E-05	8.06E-05	9.09E-05						
1.00E-02	4.71E-03	8.36E-03	9.66E-03	1.20E-02						
1.00E-01	1.12E-01	2.01E-01	3.38E-01	1.69E+00						
1.00E+00	4.05E+00	4.58E+00	4.72E+00	4.96E+00						
1.00E+01	8.28E+00	1.09E+01	1.23E+01	1.47E+01						
1.00E+02	5.56E+00	8.45E+00	1.08E+01	1.61E+01						
1.00E+03	4.56E+00	6.97E+00	8.94E+00	1.36E+01						
1.00E+04	4.38E+00	6.70E+00	8.58E+00	1.30E+01						
1.00E+05	4.36E+00	6.65E+00	8.52E+00	1.29E+01						

Table 3. Mass Attenuation Coefficients (μm) of Glass Sample	Table 3.	Mass Attenuation	Coefficients	(µm)	of Glass Sample
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Sample				Mass Attenuation Coefficient (cm ² g ⁻¹)							
Energy	1.00E-03	1.00E-02	1.00E-01	1.00E+00	1.00E+01	1.00E+02	1.00E+03	1.00E+04	1.00E+05		
S1	1.60E+04	2.12E+02	8.93E+00	2.47E-01	1.21E-01	1.80E-01	2.19E-01	2.28E-01	2.30E-01		
S2	1.35E+04	1.20E+02	4.97E+00	2.18E-01	9.20E-01	1.18E-01	1.43E-01	1.49E-01	1.50E-01		
S3	1.24E+04	1.04E+02	2.96E+00	2.12E-01	8.16E-01	9.28E-01	1.12E-01	1.17E-01	1.17E-01		
S4	1.10E+04	8.33E+01	5.92E-01	2.02E-01	6.82E-01	6.20E-01	7.38E-01	7.71E-01	7.76E-01		

from 1meV to 100keV. It has clearly observed that to some very extent, the values of mass attenuation are quite very high at low energy value; at this stage, the photoelectric effect is dominant. The mass attenuation coefficient value is evident in the Tables 3, which shows high decease in attaining minimum values at the intermediate energy range. Some photon energy move away from the intermediate range of energy are consider as Compton scattering region, the high range of energy corresponding to pair production values of mass attenuation coefficient, at very high energy the value of mass attenuation coefficient become almost constant^{6,10}.

3.3 Half Value Layer and FTIR Analysis

Half Value Layer (HVL) of the prepared glass samples at different energies was calculated from linear attenuation coefficient using equation 3 is shown in Figure 1. The simplest method to investigate the effectiveness of material is to compute its HVL value. It can be observed from Fig 1 that the HVL that was found with minimum values among

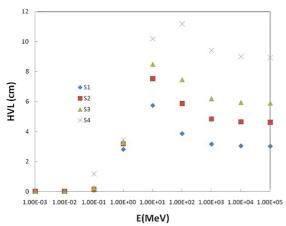


Figure 1. Plot of HVL (cm) for various samples as a function of photon energy

the glass samples is S1, which corresponds to highest lead composition (see Table 1). Minimum HVL value suggested that this composition is more effective for gamma ray shielding applications¹¹. Therefore, the HVL of S1 can be compared with corresponding HVL of the conventional shielding materials concrete (from table 4). The compositions table for the chosen concrete materials ordinary and barite concrete are given in Table 4.

The sample S1 that has minimum HVL value among all the prepared samples is plotted with corresponding HVL of standard shielding materials concrete, keeping this in mind that this glass sample (S1) is chosen and its HVL is compared with ordinary and barite concrete as shown in Figure 2. From Figure 2 it can be concluded that the sample S1 has lowest values as compared with ordinary or barite concrete. Therefore, S1 is more effective to be used be use for radiation shielding then concrete materials⁷.

The IR spectral studies (Figure 3) have been undertaken to investigate various structural groups present in our glass samples. The peaks in Figure 3 corresponding to wave numbers 545.87cm⁻¹,653.89cm⁻¹,785.05cm⁻¹ are assigned to the stretching vibration in the symmetrical of PbO₃ and ZnO spectral unit¹⁰. Some peaks are observed at 885.36cm⁻¹ it was shifted strongly to the high wave number indicating presence of Pb-O group in the sample¹³.

The peaks that were appear between 1344.7 cm⁻¹ to 1749.96 cm⁻¹ is assigned to the bond of various vibrations stretching in the borate functional unit assigned at BO₃ units. The oxygen bridges appear between one tetrahedral and one trigonal boron¹⁴. The peaks at 2364.5 to 2371.2cm⁻¹, are due to B-O symmetric stretching vibration in BO₃ units from Pyro and Ortho borate groups, these are highest intensity bands¹⁵. Some peaks are also observed with higher wavenumber in range of 3228.9 to 3458.5 cm⁻¹ can be assigned to OH group of element or H₂O.

Table 4. Chemical Compositions of Concretes

Compueto							Weight	Fractio	n						D
Concrete H	H	В	С	0	Na	Mg	Al	Si	S	K	Ca	Cr	Fr	Ba	- Density
Barite	0.0	0.01		0.34		0.002	0.004	0.01	0.099		0.0		0.004	0.42	3.5
	08	2		8		2	4	5	7		8		7	4	
Ordinary 0	0.1		0.01		0.033	0.33	33 0.0		0.0		0.014		2.2		
	0.1			9	6	0.002 8 7	7		1	4		0.014		2.3	

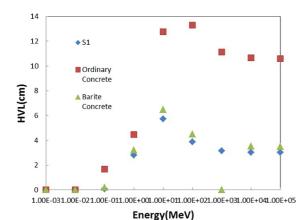


Figure 2. Plot of HVL (cm) for S1 and ordinary and barite concretes as a function of photon energy

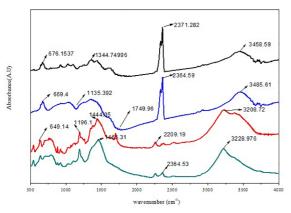


Figure 3. FTIR spectra of prepared glass samples

4. Conclusions

In this work, it is concluded that glass sample S1 has maximum mass attenuation coefficient and minimum HVL value. Furthermore, it is concluded that the attenuation properties improves with increase in lead to borate ratio. The samples containing lead shown better shielding properties in terms of less HVL value and high mass attenuation coefficient as compared with ordinary and barite concrete. FTIR studies indicate the coexistence of trigonal BO₃ and tetrahedral BO₄ units. The influence of heavy metal oxide PbO on the structural changes in borate glasses can be attributed to transformation of PbO to PbO₄ structural groups in the glass structure. Our findings suggest that glasses containing lead can serve as good radiation shielding materials as compared to concretes.

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6. References

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